

# Laser Physics 18. Pulsed lasers

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Pulsed laser operation can be obtained from a cw laser by using an external switch or modulator, e.g. a rotating disc with holes (chopper). Advantage: signal/noise ratio increases (e.g. blocking fluctuating background when measuring small signal amplitudes).

#### Disadvantage of the external modulation:

- power loss,
- peak power is the same.

Advantage of an internal modulator: short, very high peak power pulses.

Possibilities: gain or loss can be modulated!



Remember conditions of laser operation: gain condition!



**Q-switching** 

<u>Methods</u>: gain switching, *Q* – switching (or cavity damping) and mode locking.

Modulated absorber





E.g. flash lamp pumping (solid state lasers), electric current modulation (semiconductor laser), most frequently used.



During cw pumping energy is stored in the material in form of population difference – suitable laser material is needed!



$ _{0} =$	$2\pi \cdot stored energy$			_	$2\pi \cdot v$	_	V	$-2\pi\tau$	$\nu$	
Q = def	energy	loss	per	cycle	= -	$\alpha_r c$	_	$\overline{\Delta v_r}$	$=2\pi\tau_r$	v.



Methods: gain switching, **Q**-switching (or cavity damping) and mode locking.

**Q-switching** 

Cavity damping







Based on storing photons instead of population difference during the off-time and releasing them during the on-times!

In both cases modulation of the loss, but in opposite way.

**Mode locking** – differs significantly from other techniques, the phase locking of the modes provides **extremely short pulses (fs).** 

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<u>Analyses of transient effects</u> – rate equation for the photon-number density and for the inversion density

$$\frac{dn}{dt} = -\frac{n}{\tau_r} + NW_i,$$

$$W_i = \Phi\sigma(v) = nc\sigma(v),$$

$$N_t = \frac{\alpha_r}{\sigma(v)} = \frac{1}{c\tau_r\sigma(v)}$$

$$W_i = nc\frac{1}{c\tau_rN_t} = \frac{n}{\tau_rN_t}$$

$$\frac{dn}{dt} = -\frac{n}{\tau_r} + \frac{N}{N_t} \cdot \frac{n}{\tau_r}.$$

Depends on the resonator lifetime and the net photon gain arising from stimulated processes (the spontaneous emission is assumed to be small)

 $\rightarrow \sigma(v) = \frac{1}{c\tau_r N_r}, \qquad \begin{array}{l} N = N_2 - N_1 \text{ population} \\ \text{difference in unit volume!} \end{array}$ 

If  $N > N_t$ , then dn / dt > 0 and n increases! In steady state  $(dn / dt = 0) N = N_t$ .



<u>Analyses of transient effects</u> – rate equation for the photon number density and for the population difference (3-level pumping scheme)

Depends on the pumping configuration. In case of 3-level pumping scheme,  $N_3$  can be neglected because of the fast decay of level 3. If  $N_a$  is the total atomic number density and  $t_{sp} = \tau_{21}$  (there is no non-radiative decay):





<u>Analyses of transient effects</u> – rate equation for the photon number density and for the population difference (3-level pumping scheme)

$$\frac{dN}{dt} = 2R - \frac{N_a}{t_{sp}} - \frac{N}{t_{sp}} - 2\frac{N}{N_t}\frac{n}{\tau_r}$$

In steady-state in the absence of amplifier radiation the inversion density is equal to small-signal population difference,  $N_0$ :





<u>Analyses of transient effects</u> – rate equation for the photon number density and for the population difference (3-level pumping scheme)

In steady-state:

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$$\frac{dN}{dt} = 0, \quad \frac{dn}{dt} = 0 \quad \rightarrow \quad N = N_t$$
$$0 = \frac{N_0}{t_{sp}} - \frac{N_t}{t_{sp}} - 2\frac{N_t}{N_t}\frac{n}{\tau_r} \quad \rightarrow \quad n = (N_0 - N_t)\frac{\tau_r}{2t_{sp}}.$$

Steady-state photon number density of 3-level system



#### Gain switching

 $N_{0a}$ , N(t) and n(t) decrease.

Switching of the pumping rate *R* is equivalent to modulate  $N_0 = 2Rt_{sp} - N_a$ . The small-signal population difference changes from  $N_{0a}$  to  $N_{0b}!$  Time evolution of *N*(*t*) and *n*(*t*):

NOb  $t < 0, N(t) = N_{0a} < N_t$ , below the N(t) Population threshold there is no oscillation  $N_t$ Loss t = 0 the pump is turned on,  $N_{0a} \rightarrow$ N<sub>0a</sub>  $N_{0b}$ , N(t) increases, as long as  $N(t) < N_t, \ n(t) = 0$  $0 t_1$ to n(t) $\frac{dN}{dt} = \frac{N_0}{t_{sp}} - \frac{N}{t_{sp}} - 2\frac{N/n}{N_t \tau_r} = \frac{N_0 - N}{(t_{sp})} (N_{0b} - N_t) \frac{\tau_r}{2t_{sp}}$ Photon number density  $t = t_1 N(t) = N_t$ , n(t) increases, the rate  $\frac{dN}{dt} = \frac{N_0}{t_{so}} - \frac{N}{t_{so}} - 2\frac{N}{N_t}\frac{n}{\tau_r}, \quad \frac{dn}{dt} = -\frac{n}{\tau_r} + \frac{N}{N_t} \cdot \frac{n}{\tau_r}$ of increase of N(t) slows, then N(t)begins to decay because of the coupled equations. Finally  $N(t) = N_t$ . Actual shape of n(t) is obtained by numerical solution, depends on  $t_{sp}$ ,  $\tau_r$ ,  $N_t$ ,  $N_{0a}$  and  $N_{0b}$ .  $t = t_2$  the pump is turned off,  $N_{0b} \rightarrow$ 

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#### **Q-switching**

Switching the resonator loss coefficient  $\alpha_r$ , because of  $N_t = \alpha_r / \sigma(v)$  this means the modulation of  $N_t$  between  $N_{tb}$  and  $N_{ta}$ . The small-signal inversion density  $N_0(t)$  remains fixed! Evolution of N(t), n(t):

t = 0 the pump is turned on,  $N_0$ follows a step function,  $N_t = N_{ta}$ >  $N_0$ , no lasing, N(t) builds up.

 $t = t_1$  the loss is decreased,  $N_t = N_{tb} < N_{0,}$  starts the oscillation and the increase of n(t), N(t)decreases. When  $N(t) < N_{tb}$ , n(t) quickly decreases (time constant ~  $\tau_r$ ).

 $t = t_2$  the loss is reinstated,  $N_t = N_{ta}$ , N(t) again increases.



 $\frac{dN}{dt} = \frac{N_0}{t_{sp}} - \frac{N}{t_{sp}} - 2\frac{N}{N_t}\frac{n}{\tau_r}, \quad \frac{dn}{dt} = -\frac{n}{\tau_r} + \frac{N}{N_t} \cdot \frac{n}{\tau_r}$ 



<u>Q-switching</u> (cont.)

The pulse length depends on the resonator lifetime  $\tau_r$ :

$$\tau_r = \frac{1}{\alpha_r c} = \frac{2L}{c} \frac{1}{-\ln R_1 R_2}$$

A high loss and short length resonator is advantageous to use for Q-switching (e.g. with low reflectivity mirrors).

The upper level lifetime must be in the range of  $\sim ms$ .

Typical pulse length:in the range of ns - 10 ns,peak power:MW - 10 MW



#### Q-switching methods

1. Mechanical method



First realization, the rotating speed depends on  $t_{sp}$ .

E.g. rubin laser  $\tau_{21} \sim t_{sp} \sim 3 ms$ 

With the movement of one reflecting surface:  $T_{per} = 5 \text{ ms} \rightarrow 200$ revolutions/sec, 12000 revolutions/min, very high rotation speed. Attenuation of vibration and the precise alignment are the difficulties!



<u>Q-switching methods</u> (cont.)

2. Electrical solutions – electro-optic shutter

Basis: electro-optic effect. The shutter is an electro-optic crystal that becomes birefringent when electrical field is applied across the crystal, the refractive index or the phase shift can be tuned with the electric field.



When the voltage is on the shutter rotates the plane of polarization by 45°. 2x passes rotates by 90°, oscillation is blocked by the polarizer.



<u>Q-switching methods</u> (cont.)

2. Electrical solutions – electro-optic shutter (cont.)

Pockels-cell – nonlinear crystal in which an applied dc (5-10 kV) voltage induces a change in the crystal's refractive index.

 $\begin{array}{c} \text{KDP} (\text{KH}_2\text{PO}_4) \\ \text{LiNbO}_3 \end{array} \right)$ 

visible and near-infrared

CdTe middle-infrared

Kerr-cell – normally isotropic liquid becomes birefringent by aligning the molecules with electric field

e.g. liquid nitrobenzene ( $C_6H_5NO_2$ ), disadvantage – toxic and >10 kV high voltage is necessary!



Q-switching methods (cont.)

2. Electrical solutions – acousto-optic shutter acousto-optic crystal in the resonator, e.g. a quartz crystal

Traveling acoustic waves in the crystal. The acoustic wavelength is

 $\lambda_a = v / v_a$ , *v* is the velocity of sound,  $v_a$  is the frequency of the RF field.

The light is diffracted on the traveling wave (eff. can be 50%, oscillation stops because of the high loss).





<u>Q-switching methods</u> (cont.)

2. Electrical solutions – acousto-optic shutter (cont.)

Diffraction only in definite angles according to the Bragg condition (like in crystals the x-ray diffraction)



After switching off the RF field the diffraction disappears and the laser oscillation starts. Repeated Q-switching is possible.



<u>Q-switching methods</u> (cont.)

3. Passive Q-switching



The saturable absorber causes high loss at the beginning. With increasing flux density the absorber saturates and becomes transparent.

Suitable materials	BDN dye (4-dimetil-aminodithiobenzil-nikkel) in ethanol
	for 1.06 µm (Nd:YAG laser)
	SF <sub>6</sub> gas for 10.6 µm (CO <sub>2</sub> laser)
	semiconductor layer on mirror (SESAM – semiconductor saturable absorber mirror)
Important:	saturation flux density must be low saturation time must be low (~ μs)
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Method of cavity damping

Instead of the modulation of the mirror transmittance an acousto-optic deflector can be used:





#### Mode locking

Ultra short pulse generation by the synchronization of phases when large number of longitudinal modes oscillate. Without synchronization random fluctuating output:





<u>Mode locking</u> – theory

The sum of *M* longitudinal modes with  $\phi$  fixed phase and with equal frequency difference  $\Delta v_n$  (large operational bandwidth is necessary, e.g. dye or solid-state laser):

$$E(t) = \sum_{k=-M/2}^{M/2} E_k \cdot e^{i2\pi(v_0 + k\Delta v_n)t + i\phi}, \quad \Delta v_n = \frac{c}{2L}$$

Simplification – equal amplitudes:  $E_k = E_0$ , sum of geometric series:

$$E(t) = E_0 \cdot e^{i2\pi v_0 t + i\phi} \sum_{k=-M/2}^{M/2} \cdot e^{i2\pi k \Delta v_n t} = E_0 \cdot \frac{\sin(M\pi \cdot t \cdot \Delta v_n)}{\sin(\pi \cdot t \cdot \Delta v_n)} \cdot e^{i2\pi v_0 t + i\phi}$$
$$I(t) = |E_0|^2 \cdot \frac{\sin^2(M\pi \cdot t \cdot \Delta v_n)}{\sin^2(\pi \cdot t \cdot \Delta v_n)}$$



<u>Mode locking</u> – theory (cont.)

$$I(t) = |E_0|^2 \cdot \frac{\sin^2(M\pi \cdot t \cdot \Delta v_n)}{\sin^2(\pi \cdot t \cdot \Delta v_n)}, \quad \Delta v_n = \frac{c}{2L}$$

Pulse maxima occur when  $\pi \cdot t \cdot \Delta v_n = 0$ ,  $\pi$ ,  $2\pi$ , ...,  $q\pi$ , q is integer (the denominator is 0):

$$I(t)_{lim} = \lim_{\pi \cdot t \cdot \Delta v_n \to 0} \left| E_0 \right|^2 \cdot \frac{\sin^2 \left( M\pi \cdot t \cdot \Delta v_n \right)}{\sin^2 \left( \pi \cdot t \cdot \Delta v_n \right)} = \lim_{\pi \cdot t \cdot \Delta v_n \to 0} \left| E_0 \right|^2 \cdot \frac{M^2 \left( \pi \cdot t \cdot \Delta v_n \right)^2}{\left( \pi \cdot t \cdot \Delta v_n \right)^2} = M^2 \left| E_0 \right|^2$$

$$I(t)_{max} = M^2 \big| E_0 \big|^2$$

Maximum intensity is *M* times the average intensity!!!

Distance of maxima:  $\pi \cdot t \cdot \Delta v_n = \pi \rightarrow$ 

$$t_{sep} = \frac{1}{\Delta v_n} = \frac{2L}{c}$$

Running time!!

Minimum:  $M \pi \cdot t \cdot \Delta v_n = \pi \rightarrow \begin{bmatrix} t_p \cong \frac{1}{M \Delta v_n} = \frac{1}{B} \end{bmatrix}$  ~ inversely depends on the operational bandwidth!!

Pulse length: ~ the distance of the first minimum from the maximum place Laser Physics 18



Mode locking (cont.)

The intensity is a periodic function in time, its characteristics:

- periodic maxima according to the running time in the resonator (2L/c in time and 2L distance in space)
- Pulse length inversely proportional to the operational bandwidth of the amplifier
- peak intensity = average intensity x the number of coupled modes

$$I(t) = |E_0|^2 \cdot \frac{\sin^2(M\pi \cdot t \cdot \Delta v_n)}{\sin^2(\pi \cdot t \cdot \Delta v_n)}$$
  

$$t_p \approx \frac{1}{M\Delta v_n} = \frac{1}{B}$$
  

$$B = 100 THz \rightarrow t_p \sim 10^{-14} s = 10 fs$$





In the reality the amplitudes are different, their form depend on the shape of the gain coefficient.

$$t_{\rho} \cong rac{eta}{M \Delta v_{n}},$$

 $\beta$  ~1, depends on the shape of the gain coefficient! For inhomogeneous amplifier:  $\beta$  =0.441.

~200 ps pulse train of a mode locked Nd:YAG laser.





<u>Mode locking</u> – practical methods

- Active mode locking, external power source is used for the control of the switch: electro-optic or acousto-optic cell in the resonator (like for Q-switching), or synchronized pumping (pumping pulses with frequency c/2L, difficult to realize)
- Passive mode locking, no external power source, a saturable absorber or material with nonlinear variation of the refractive index is applied most frequently close to one mirror. Pulse with sufficiently large irradiance saturates the absorber, therefore goes through without loss. The recovery time of the absorber must be shorter than the roundtrip time in the resonator!