

(08. 07.)

Kis. Fiz. 3. Gyak.

Márkus Bence

xymarkus@gmail.com

(1) - 463 - 1215

Termodinamika

B-M, G-L

Állapotjelző: leírja a rendszer pill.-nyi állapotát

↳ intenzív: kiegyenlítődnek a foly. során: p, T, μ

↳ extenzív: összeadódnak a foly. során: U, V, S

Állapotegyenletek:

$$\frac{1}{273K} = \frac{1}{T_2}$$

B-M: $T = \text{áll.}; pV = \text{áll.}$

↓ hőm. küi. (°C)

G-L II: $V = \text{áll.}, \frac{p}{T} = \text{áll.} \rightsquigarrow p' = p_0(1 + \beta \Delta T)$

G-L I: $p = \text{áll.}, \frac{V}{T} = \text{áll.} \rightsquigarrow V = V_0(1 + \beta \Delta T)$

$p_0, V_0, 0^\circ\text{C}$

↓ izov

p', V_0, t

↓ izot

p, V, t

$$p'V_0 = p \cdot V_0(1 + \beta \Delta T) = pV$$

$\frac{R}{N_A}$ Boltzmann-áll.

$$\frac{p_0 V_0}{T_2} (T_2 + t) = pV \quad \Rightarrow \quad pV = nRT = \frac{U}{N_A} RT = U k_B T$$

Kinematikus gázelmélet:

abs. rugalmas
ütközés

Feltételezés: - ütközéskor csak imp. átadás \rightarrow hard wall \Rightarrow

- \Rightarrow impulzus előjelet vált
- sok atom, sok ütközés
- kocka alakú edény, L oldalhossz



- 1 atom, Δt idő, ütközés száma?

2 ütk. közt $\Delta s = 2L$ \downarrow $N = \frac{v_x \Delta t}{2L} = \frac{|p_x| \Delta t}{2L}$

- 1 ütközés alatt átadott impulzus?

$$dp_x = 2|p_x|$$

- Δt idő alatt átadott impulzus $\Rightarrow N \cdot dp_x = |p_x|^2 \frac{\Delta t}{mL}$

További feltételezések:

- függetlenek
 - \emptyset k.
 - pontszerűek
- $b(-f=3)$

• átlagolás N db részecshite: $\sum_{k=1}^N \frac{|p_{kx}|^2 \Delta t}{mL} = F \Delta t = n L^2 \Delta t$

$\frac{F}{\Delta t} = \frac{F}{A} = n [L^3 = V]$

$$n = \frac{1}{V} \sum_{k=1}^N \frac{|p_{kx}|^2}{m}$$

ezt átlagoljuk

• átlagos impulzus: $\overline{p_x^2} = \frac{1}{N} \sum_{k=1}^N p_{kx}^2$

$$n = \frac{V}{V} \frac{\overline{p_x^2}}{m}$$

• nincs kitüntetett irány: $\overline{p_x^2} = \overline{p_y^2} = \overline{p_z^2} = \frac{1}{3} \overline{p^2}$

• tegyük a nyomás: $p = \frac{V}{V} \frac{\overline{p^2}}{3m} = \frac{2}{3} \frac{V}{V} \frac{\overline{p^2}}{2m}$

$$\varepsilon = \frac{p^2}{2m} = \frac{1}{2} \frac{mv^2}{m} = \frac{1}{2} mv^2 \quad [\text{kinetikus energia}]$$

$$\bar{\varepsilon} = \frac{1}{N} \sum_{k=1}^N |p_k|^2 / 2m$$

$$\bullet \quad n = \frac{2}{3} \frac{N}{V} \frac{\bar{p}^2}{2m} = \frac{2}{3} \frac{N}{V} \bar{\varepsilon}$$

$$\bullet \quad pV = Nk_B T \quad \Rightarrow \quad \frac{2}{3} \bar{\varepsilon} = k_B T \quad \Rightarrow \quad \boxed{\bar{\varepsilon} = \frac{3}{2} k_B T}$$

↑ kinetikus energia-
átlag

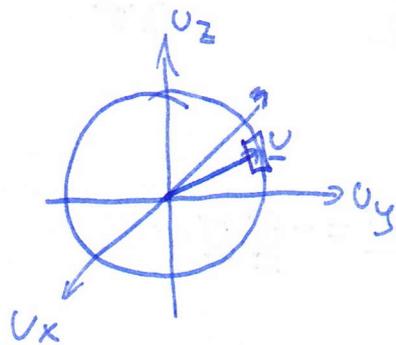
1/1 N részecske

belső E: $U = N\bar{\varepsilon} = N \frac{f}{2} k_B T$

$$pV = \frac{2}{3} N\bar{\varepsilon} = \frac{2}{3} U \quad \rightarrow \quad \boxed{n = \frac{2}{3} \frac{U}{V}}$$

TRANSPORT:

molekula \rightarrow random mozgás kérdés: kül. mennyiségel
hogyan változik?



$dP =$ az a valószínűség, hogy a mol.-a hirtelen
adott irányba (azaz \underline{v} vektor-) az
adott irány körüli $d\Omega$ térszögben
van?

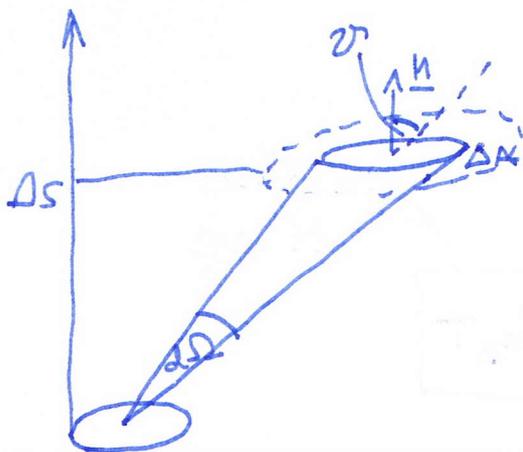
$$dP = \frac{dA}{4v^2\pi} = \frac{d\Omega}{4\pi} \quad dA = r^2 \sin\theta d\theta d\varphi \rightarrow d\Omega = \sin\theta d\theta d\varphi$$

$$dN = N dP = N \frac{d\Omega}{4\pi}$$

kérdés: hány molekula ütközik adott idő alatt adott
felületen?

$$(v, v+dv) \rightarrow dN_v \quad dN_{v, \theta, \varphi} = dN_v \frac{d\Omega}{4\pi}$$

kérdés: $A \rightarrow B$ -be mennyi részecske jut el?



$\Delta A, \Delta t$
 max. Δs táv.-ra lehetnek
 $\Delta s = v \cos \varphi \Delta t$
 $\Delta U = \Delta t \Delta s$

ΔA -n mennyi molekula halad át?

$$\Delta z_{v \varphi} = dN_{v \varphi} \frac{\Delta U}{V} = dN_v \frac{\Delta A \Delta t}{4\pi V} v \cos \varphi \sin \varphi d\varphi$$

$$n_v = \frac{N}{V}$$

haladás irányában van

$$\Delta z_{\Delta A, \Delta t} = \frac{\Delta A \Delta t}{4\pi} \left(\frac{n_v}{N} \int_0^{v_{max}} v dN_v \right) \left(\int_0^{\pi/2} \cos \varphi \sin \varphi d\varphi \right) \int_0^{2\pi} d\varphi$$

sebesség átlag \bar{v} $\frac{1}{2}$ 2π

$$\Delta z_{\Delta A, \Delta t} = \frac{1}{4} n_v \bar{v} \Delta A \Delta t$$

$$\underline{j} = \frac{1}{4} n_v \bar{v}$$

molekula
áramlás
sűrűsége

hajtóerő

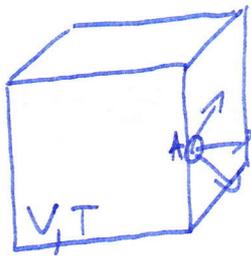
OnSager: $\underline{j} = \sum_j L_{ij} \underline{x}_j$

$$\underline{j}_e = \underline{\sigma} \underline{E} = -\underline{\sigma} \underline{\nabla} \phi$$

$$\underline{j}_q = -\lambda \underline{\nabla} T$$

$$\underline{j}_n = -D \underline{\nabla} n$$

1/6



$$\frac{dN}{dt} = \frac{1}{4} n_v A \bar{v}$$

↓
Falmak átáramlása

A lyuk ha arra vágunk
kiegészítjük

- részecskeszáma változik? $\rightarrow \frac{dN}{dt} = V \frac{dn_v}{dt} = - \frac{1}{4} n_v \bar{v} A$
- $\Delta t = ?$ ha $P_2 = \frac{1}{2} P_1$

$$\frac{dn_v}{n_v} = - \frac{A \bar{v}}{4V} dt \quad / \int$$

$$\int \frac{1}{n_v} dn_v = - \int \frac{A \bar{v}}{4V} dt$$

$$\ln \frac{n_v}{n_{v_0}} = - \frac{A \bar{v}}{4V} t = - \frac{t}{\tau}$$

$$n_v(t) = n_{v_0} e^{-\frac{t}{\tau}}$$

$$N(t) = V n_v(t)$$

$$n_v(T_{1/2}) = \frac{n_{v_0}}{2} \quad n_v(\tau) = \frac{n_{v_0}}{e}$$

$$\frac{n_{v_0}}{2} = n_{v_0} e^{-\frac{T_{1/2}}{\tau}} \Rightarrow T_{1/2} = \tau \ln 2$$

1/7

T=all. V ⁽¹⁾	T=all. V ⁽²⁾
H ₂ P _{kerd}	H ₂ 2P _{kerd}

$P = \frac{3}{2} P_{kerd}$ lesz az. egyensúlyi nyomás.

áreg

$$N_{lyuk} = \frac{1}{4} n_v A \bar{v}$$

$$\frac{dN^{(1)}}{dt} = -\frac{1}{4} n_v^{(1)} \bar{v} A + \frac{1}{4} n_v^{(2)} \bar{v} A$$

$$N^{(2)} = N - N^{(1)}$$

↓ kiáramlás ↓ visszaáramlás

$$\frac{dN^{(2)}}{dt} = -\frac{dN^{(1)}}{dt}$$

$$\frac{V^{(1)} \frac{dn_v^{(1)}}{dt}}{dt} = -\frac{1}{4} \bar{v} A \left(1 + \frac{V^{(1)}}{V^{(2)}}\right)$$

$$\bar{v}^{(1)} = \bar{v}^{(2)} \text{ mert } T^{(1)} = T^{(2)} !$$

$$V^{(1)} \frac{dn_v^{(1)}}{dt} = -\frac{1}{4} \bar{v} A \left(1 + \frac{V^{(1)}}{V^{(2)}}\right) n_v^{(1)} + \frac{1}{4} \bar{v} A \frac{N}{V^{(2)}}$$

egyensúly: $\left. \frac{dn_v^{(1)}}{dt} \right|_{\text{egyens.}} = 0 \rightarrow \left(1 + \frac{V^{(1)}}{V^{(2)}}\right) n_v^{(1)} = \frac{N}{V^{(2)}}$

u tartályra

$$n_v^{(1)} = \frac{N}{V^{(1)} + V^{(2)}} = n_v^{(2)}$$

nyomás? \Rightarrow

$$pU = N k_B T$$

$$p = \frac{N^{(1)} + N^{(2)}}{V^{(1)} + V^{(2)}} k_B T = \left[\sum_i \frac{N_i}{V_i} k_B T \right]$$

$$P_{kerd} = \frac{N^{(1)}}{V^{(1)}} k_B T = \frac{N^{(2)}}{2V^{(2)}} k_B T$$

$$V^{(1)} = V^{(2)} = V$$

$$\hookrightarrow N_{kerd}^{(1)} = \frac{1}{2} N_{kerd}^{(2)} = \frac{N}{3} \Rightarrow$$

$$\boxed{P = \frac{3}{2} P_{kerd}}$$

1/

$$m_{H_2} = 2 \frac{g}{mol}$$

$$m_{O_2} = 32 \frac{g}{mol}$$

Dalton tv: $P_{veg} = P_{veg H_2} + P_{veg O_2}$

$$\frac{dN_H^{(1)}}{dt} = -\frac{1}{4} n_{vH}^{(1)} \bar{v}_H A + \frac{1}{4} n_{vH}^{(2)} A \bar{v}_H$$

$$\frac{dN_H^{(1)}}{dt} = 0$$

$$\frac{dN_O^{(1)}}{dt} = -\frac{1}{4} n_{vO}^{(1)} \bar{v}_O A + \frac{1}{4} n_{vO}^{(2)} A \bar{v}_O$$

$$N_H^{(2)} = N_H - N_H^{(1)}$$

z.F.: $n_{vH}^{(1)} k_{vezd} = n_{vH} k_{vezd}$

$$n_{vH}^{(2)} k_{vezd} = 0$$

Előző fejelet:

$$pU = nRT = N k_B T$$

$$pU = \frac{2}{3} U = \frac{2}{3} N \bar{\epsilon}$$

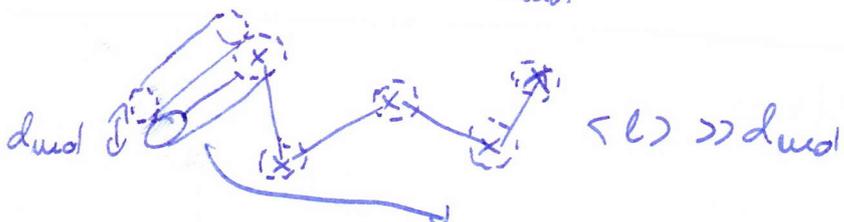
$$\dot{J}_{\text{mol}} = \frac{1}{4} n_v \bar{v}$$

$$\dot{J}_n = -D \nabla n = -D \nabla c$$

Szabad úthozz: $\langle l \rangle$ átl. nélkül megtett táv

molekula \rightarrow gömb \rightarrow d_{mol} 

átlk. \rightarrow rug. 



Δt : $S = \bar{v} \Delta t$ henger térfogatán belüli csúcsokba átlk.

átlk. azokból: $\Delta U = d_{\text{mol}}^2 \pi S = d_{\text{mol}}^2 \pi \bar{v} \Delta t$

hatáskeresztmetszet:

$$S = d_m^2 \pi = b^2 \pi$$

$$dS = 2\pi d_m dd_m = 2\pi b db$$

Δt átlk. száma: $\Delta z = \Delta U n_v = n_v d_m^2 \pi \bar{v} \Delta t$

\downarrow
átlk. száma

$$\left[\begin{array}{l} 2 \text{ átlk. eltelt idő:} \\ \Delta \tau = \frac{\Delta t}{\Delta z} = \frac{1}{n_v d_m^2 \pi \bar{v}} \end{array} \right]$$



$$\langle l \rangle = \Delta \tau \bar{v} = \frac{1}{n_v d_m^2 \pi \sqrt{2}}$$

a többi mol.
is zörög

$$p = \frac{N k_B T}{V} = n k_B T$$

$$\hookrightarrow n = \frac{p}{k_B T}$$

$$\langle l \rangle = \frac{k_B T}{\sqrt{2} \pi d_{\text{m}}^2 p}$$

T1/4 $V = 1 \text{ l gomb}$ $V = \frac{4r^3\pi}{3} \Rightarrow R = 0,062 \text{ m}$

$T = 300 \text{ K}$

$\text{H}_2 \rightarrow d_{\text{m}} = 2 \text{ \AA}$

$p_{\text{max}} = ?$ hogy $\langle l \rangle > d_{\text{edény}}$

$$\frac{k_B T}{\sqrt{2} \pi d_{\text{m}}^2 p}$$

$$p < \frac{k_B T}{2\sqrt{2} R d_{\text{m}}^2 \pi}$$

$$p < 0.188 \text{ Pa}$$

DIFFÚZIÓ

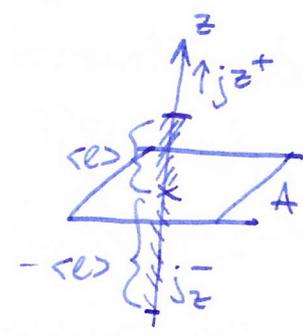
- magasabb konc. ↔ alacsonyabb
- |j| függ az átvezések számától

Tfh: d, u, \bar{u} azonosak $\Rightarrow \langle l \rangle$ is azonos

1D: $n = n(z)$; val Δt fel Δz

sűrűség kül.

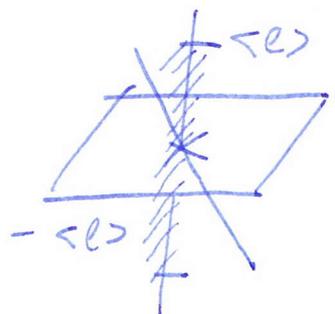
$$j_{\text{diff}} = j_z^+ - j_z^- = \frac{1}{4} \bar{u} (n^+ - n^-)$$



$j_{\text{mol}} = \frac{1}{4} n \bar{u}$ + f.h. linearisan vált. $\langle l \rangle$ en belül

$$n^+ \approx n(z - \langle l \rangle)$$

$$n^- \approx n(z + \langle l \rangle)$$



$$n_v^+ - n_v^- \approx n_v [(z - \langle l \rangle) - (z + \langle l \rangle)] = - \frac{dn_v}{dz} \cdot 2 \langle l \rangle$$

$$\begin{cases} n_v^+ \approx n_v(z - \langle l \rangle) \\ n_v^- \approx n_v(z + \langle l \rangle) \end{cases}$$

$$j_{\text{diff}} = - \frac{1}{2} \bar{u} \langle l \rangle \frac{dn_v}{dz}$$

$\frac{1}{3}$ vágyában

$$j_{\text{diff}} = - D \nabla n \quad (\text{Fick I.})$$

↑
diff.-ös áll.

ideális gáz $D = \frac{1}{3} \bar{u} \langle l \rangle$

Viszkozitás

áramlás irányába \perp vált. a seb.

$u_x(z) = \text{áram. seb.} - e$

ΔA felület
(átmenni imp.)?

$\Delta p \uparrow$
 \downarrow imp. addódik át
a kül. részek
közé

u_x(z) ut
globalis irány

$$\Delta p = \Delta p_x^+ - \Delta p_x^- = \eta (u_x^+ - u_x^-)$$

$$j_{\text{imp}}^z = \frac{1}{4} n_v \bar{u} m (u_x^+ - u_x^-)$$

$$u_x^+ - u_x^- \approx u_x (z - \langle l \rangle) - u_x (z + \langle l \rangle) = - \frac{du_x}{dz} \cdot 2 \langle l \rangle z$$

$$j_{\text{imp}}^z = - \frac{1}{3} n_v \bar{u} m \langle l \rangle \frac{du_x}{dz}$$

η : viszkozitás

Newton-tv.: $j_{\text{imp}}^z = - \eta \frac{du_x}{dz}$

ideálisg: $\eta = \frac{1}{3} n_v \bar{u} \langle l \rangle m$

T1/5

ideális, D, η

$$\eta(T, U) \\ D(T, U)$$

a, T = állandó.

b, p = állandó.

$$P = \frac{1}{3} \langle e \rangle \bar{U}$$

$$n_U = \frac{U}{V}$$

$$\langle e \rangle = \frac{1}{\sqrt{2} n_U \sigma}$$

$$\bar{v} = \sqrt{\frac{8 k_B T}{m \pi}} \quad \mu_{x-z}$$

$$D(T, U) = \frac{1}{3} \frac{U}{\sqrt{2} U \sigma} \sqrt{\frac{8 k_B T}{m \pi}}$$

$$\eta(T, U) = + \frac{1}{3} \frac{1}{\sqrt{2} \sigma} \sqrt{\frac{8 k_B T}{m \pi}} \quad m$$

a, T = állandó.

U → n · U
növeljék

D ∼ U

η ∼ 1 ∼ U⁰ (nem függ U-tól)

D → n · D

η → η

b, p = állandó.

$$P = \frac{U}{V} k_B T$$

$$\sqrt{T} \sim \sqrt{pV} \sim \sqrt{U}$$

$$D \sim U^{3/2}$$

$$\eta \rightarrow U^{1/2}$$

$$D \rightarrow n^{3/2} D$$

$$\eta \rightarrow n^{1/2} \eta$$

Hőáram/Hővezetés

$$T = T(z)$$

$$\bar{E} = \frac{f}{2} k_B T$$

linearizálás

$$j_z^{hő} = \frac{1}{4} n_U \bar{v} (\bar{E}_+ - \bar{E}_-) \stackrel{\downarrow}{=} \frac{f k_B}{8} n_U \bar{v} (T_+ - T_-) \stackrel{\downarrow}{\sim} - \frac{f}{6} k_B n_U \langle e \rangle \frac{dT}{dz}$$

hőáramsűrűség:

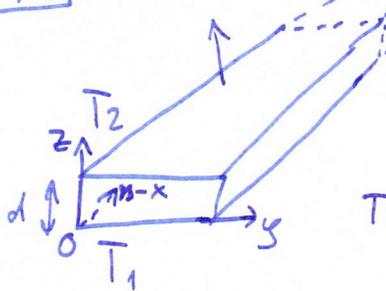
$$j_q = -\lambda \nabla T$$

hővezetési eh.

$$\text{ideális gáz: } \lambda = \frac{f}{6} k_B n_U \bar{v} \langle e \rangle \propto \frac{1}{6} \sqrt{\frac{T}{m}}$$

T1/g

eggs szedek felületc: A



$$\lambda(T, \epsilon) = \lambda \quad (\text{nem függ } T\text{-től, } \epsilon\text{-től})$$

$$T(z)$$

$$\text{KF: } T(0) = T_1$$

$$T(d) = T_2$$

$$j_Q = -\lambda \frac{dT}{dz}$$

$$J_Q = \int dt j_Q = \frac{dQ}{dt} = \text{vidőegység adott felületen átvitt hő}$$

$$j_Q = -\lambda \frac{dT}{dz}$$

$$J_Q = \int dt j_Q = \frac{dQ}{dt}$$

$$\boxed{\frac{dQ}{dt} = -\lambda A \frac{dT}{dz}}$$

hővez. alap egyenlete

stac. eset \rightarrow hő ϕ harmonizál fel (kiadakt a veigso⁴ hőm.: i profil)

$$J_Q = \text{áll.} \rightarrow \frac{dQ}{dt} = \text{áll.} \Rightarrow -\lambda A \frac{dT}{dz} = \text{áll.} \Rightarrow \frac{dT}{dz} = \text{áll.} = c$$

$$\frac{dT}{dz} = c_T$$

$$dT = c_T dz \quad / \int$$

$$\boxed{T(z) = c_T z + T(0)}$$

$$T(0) = T_1 \quad T(d) = T_2$$

$$T(d) = T_2 = T_1 + c_T d$$

$$\underline{\underline{c_T = \frac{T_2 - T_1}{d}}}$$

$$\boxed{T(z) = \frac{T_2 - T_1}{d} z + T_1}$$

(08.21.)

Hővezetés alap tu.-c

T1/10

$$z = 5 \text{ cm}$$

$$T_e = -10^\circ\text{C}$$

$$T_o = 0^\circ\text{C}$$

$$L_o = 335 \frac{\text{J}}{\text{g}}$$

$$\lambda = 21 \cdot 10^{-2} \frac{\text{J}}{\text{cm} \cdot \text{C}}$$

$$\rho = 0,82 \frac{\text{g}}{\text{cm}^3}$$

mittkor

$$\frac{dQ}{dt} = -\lambda \frac{dT}{dz} ; T(z) = T_1 + \frac{T_2 - T_1}{d} z = C + C'z \quad \forall z(t)$$

$$\frac{dT}{dz} = \frac{T_o - T_e}{z(t)} \quad \left[dQ = -L_o dm = -L_o \rho A dz \right]$$

⇓

$$L_o \rho A \frac{dz}{dt} = \lambda A \frac{T_o - T_e}{z(t)}$$

+0) => kezdő minőség

$$\int z dz = \frac{T_o - T_e}{L_o \rho} \lambda dt + C$$

$$\frac{z^2}{2} = \frac{\lambda}{L_o \rho} (T_o - T_e) t \rightsquigarrow t(z) = \frac{\rho L_o}{2 \lambda (T_o - T_e)} z^2 + (5 \text{ cm}) = 5,1 \text{ óra}$$

T1/11

T_o
 $T_1 > T_o$
 m, c



$$j_Q = \kappa (T - T_o)$$

hővez. alap tu.-c:

$$\frac{dQ}{dt} = A \kappa (T - T_o)$$

$$dQ = ? \quad dQ = \underbrace{\frac{1}{c} dm}_{\text{hőelvadás}} dt$$

hűl

$$-c m \frac{dT}{dt} = A \kappa (T - T_o) \quad \tilde{T} = (T - T_o)$$

$$d\tilde{T} = dT \quad \text{mert } T_o \text{ egy konst}$$

$$-c m \frac{d\tilde{T}}{dt} = +\kappa \tilde{T}$$

$$\ln \tilde{T} = -\frac{\kappa A}{c m} t + \ln C$$

$$T - T_o = e^{-\frac{\kappa A}{c m} t} C \quad \text{k.f.: } T(0) = T_1 \rightsquigarrow C = T_1 - T_o$$

$$\int \frac{d\tilde{T}}{\tilde{T}} = -\frac{\kappa A}{c m} dt$$

$$T(t) = T_o + (T_1 - T_o) e^{-\frac{\kappa A}{c m} t}$$

Fundamentális termodinamika

↓
tapasztalati úton
építjük fel

0. Főtétel: $A \Leftrightarrow B \Rightarrow A \Leftrightarrow C$
 $B \Leftrightarrow C$

Tap: • Testen végzett mechanikai munka elvissz \rightarrow hővé alakul
• Meleg testtel munkát lehet végeztetni

hőmérséklet emelkedés \sim hőtartalom \sim hő (energia)

\rightarrow környezettől elzárt \rightarrow hőszigetelt \rightarrow adiabatikusán elszigetelt

\hookrightarrow meghatározott állapotváltozáshoz munka rendelhető

$$U_A, U_B$$

$$W_{\text{adiab.}} = \Delta U$$

$$\delta W_{\text{adiab.}} = dU$$

\rightarrow (ha nem elszigetelt) \Rightarrow munka: makroszkop. átadott ϵ
hő: $\epsilon - \nu \quad \epsilon$

$$\delta Q = \delta W_{\text{adiab.}} - \delta W$$

\Rightarrow 1. Főt. $dU = \delta W + \delta Q$ (\Leftarrow energiamegmar.)

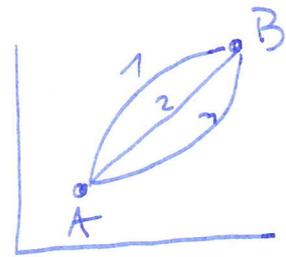
belső E
vált.-a

felvett/leadott hő
(előjel függő)

általánosan végzett munka $\Rightarrow \delta W_{\text{általános}} = -\delta W_{\text{rendszer által}}$

d = állapotjelzők alapján e.é.-en meghatározható a megvalh.

δ = állapotvált. útjától is függ



$$dU = dU_1 = dU_2 = dU_3$$

$$\delta W_1 \neq \delta W_2$$

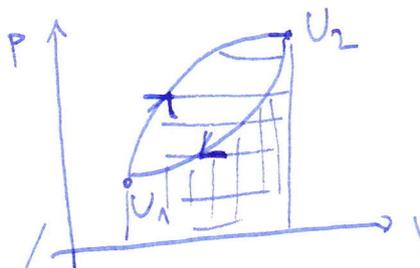
Körfolyamat

$$\boxed{dU = 0} \rightarrow \delta Q + \delta W = 0$$

$$\delta Q = -\delta W$$

Munkák:

mech.-i munka: térfogati munkavégzés



$$\delta W_{\text{mech.}} = -p dV$$

$$W_{\text{mech.}} = - \int_{V_1}^{V_2} p dV$$

(Felső útra, mert $V_1 \rightarrow V_2$)

feltételérés:

$$\Delta p \ll P_{\text{abs.}} \approx P_{\text{húts.}}$$

$$p \approx \text{álland.}$$

} \Rightarrow reverzibilisnek tekinthető emiatt

rendszer által végzett munka a 2 terület kül.-e

Hő:

$$\delta Q \sim dT$$

$$\delta Q = K dT$$

$K = ? \rightarrow$ hőkapacitás (sok mindentől függ)

$$K = c \cdot m$$

\hookrightarrow fajhőanyagra jell.

$\kappa = C n \Rightarrow$ gázok tömegét vezéző mérték:
 \hookrightarrow moláris hőkap.

$$C = \frac{1}{n} \frac{\delta Q}{dT} = \frac{1}{n} \frac{dU + p dV}{dT} \Rightarrow \text{függ az úttól, mert tartalmazza a munkát is}$$

$C_v =$ áll. térf.-on mért fajhő $\Rightarrow dV = 0$

$$\delta Q = dU = n C_v dT \quad dU = \frac{\partial U}{\partial T} \Big|_V dT + \frac{\partial U}{\partial V} \Big|_T dV \quad \text{dV=0 akkor elhanyagolható}$$

\downarrow
d miatt
teljes differenciál

(láncszabály, teljes deriváltakra való)

$$C_v = \frac{1}{n} \frac{\partial U}{\partial T} \Big|_V$$

$C_p =$ áll. nyom.-on mért fajhő $\Rightarrow dp = 0$

$$C_p = \frac{1}{n} \frac{dU + p dV}{dT} \Big|_p$$

entalpia: $H = U + pV$ (Legendre-transzformáció)

$$dH = dU + d(pV) + p dV$$

$dp = 0$

$$C_p = \frac{1}{n} \frac{\partial H}{\partial T} \Big|_p \left(= \frac{1}{n} \frac{\delta Q}{dT} \Big|_p \right)$$

c_p, c_v nem fgtl.-ek

$$dU = \left. \frac{\partial U}{\partial T} \right|_V dT + \left. \frac{\partial U}{\partial V} \right|_T dV$$

$$\delta Q = dU + p dV = \underbrace{\left. \frac{\partial U}{\partial T} \right|_V}_{n c_v} dT + \underbrace{\left. \frac{\partial U}{\partial V} \right|_T}_{dV \left[\left. \frac{\partial U}{\partial V} \right|_T + p \right]} dV + p dV$$

$$c_p = \frac{1}{n} \left. \frac{\delta Q}{\delta T} \right|_p = \frac{1}{n} \left\{ n c_v + \left[\left. \frac{\partial U}{\partial V} \right|_T + p \right] \left. \frac{\partial V}{\partial T} \right|_p \right\}$$

$$c_p \cdot c_v = \frac{1}{n} \left[\left. \frac{\partial U}{\partial V} \right|_T + p \right] \left. \frac{\partial V}{\partial T} \right|_p$$

$$c_p - c_v = R$$

izobár ténf. hőtág. e.h.

$$\beta_p = \frac{1}{V} \left. \frac{\partial V}{\partial T} \right|_p$$

$$c_p - c_v = \frac{1}{n} \left[\left. \frac{\partial U}{\partial V} \right|_T + p \right] \beta_p V$$

$$c_p = c_v + R = \frac{f+2}{2} R$$

$$\gamma = \frac{c_p}{c_v} = \frac{f+2}{f}$$

↳ id.gáz. u-ból

A'LLAPOTVÁLTOZÁSOK

(id. gázok)

i, izot; $T = \text{all.}$

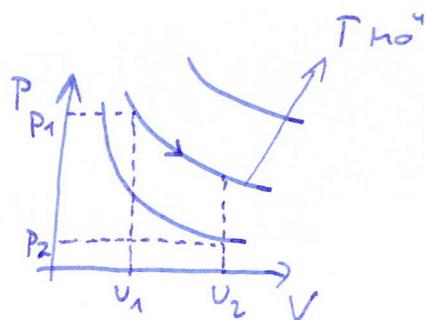
$$pV = nRT = \text{all.} \rightarrow p(V) \sim \frac{1}{V}$$

ideális: $U(T) = U = \text{all.} \quad \underline{dU = 0}$

végzett munka:

$$\left[W = - \int_{V_1}^{V_2} p dV = - \int_{V_1}^{V_2} \frac{nRT}{V} dV = -nRT \ln \frac{V_2}{V_1} = -nRT \ln \frac{P_1}{P_2} \right]$$

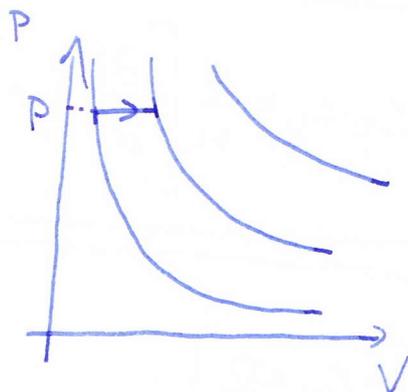
$$Q = -W$$



ii, izop; $p = \text{all.}$

$$\left[W = p(V_2 - V_1) \right]$$

$$Q = U_2 - U_1 + p(V_2 - V_1) = nC_p(T_2 - T_1)$$



iii, adiabatikus \rightarrow hőcsere $\int Q = 0$

$$dU + p dV = 0$$

$$nC_v dT + p dV = 0$$

\Downarrow

$$nC_v dT + nRT \frac{dV}{V} = 0$$

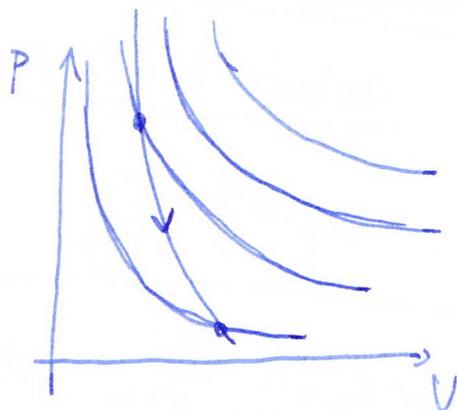
$$R = C_p - C_v; \quad \gamma = \frac{C_p}{C_v}$$

$$\frac{dT}{T} + (\gamma - 1) \frac{dV}{V} = 0 \quad / \cdot$$

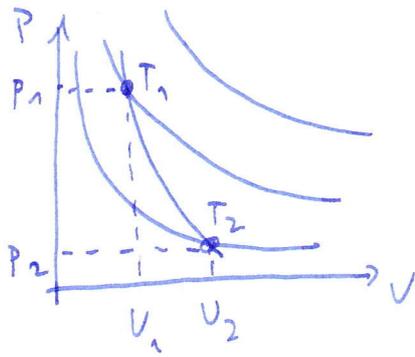
$$\ln T + (\gamma - 1) \ln V = \text{const.}$$

$$\boxed{TV^{\gamma-1} = \text{const.}}$$

$$pV^\gamma = \text{const.}$$



Biz.: (adiabata meredekebb mint izoterma)



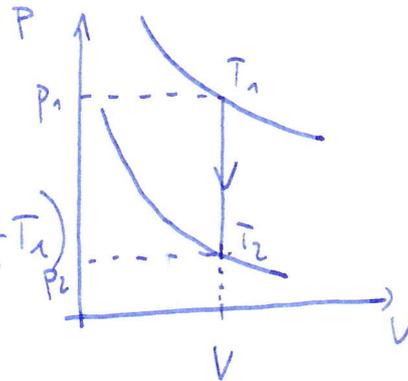
izot: $pU = p_0 U_0$
 adiab: $pU^\gamma = p_0 U_0^\gamma$

meredekség: $\left. \frac{\partial p}{\partial V} \right|_T = -\frac{p_0}{U_0}$

$\left. \frac{\partial p}{\partial V} \right|_{\text{adiab.}} = -\gamma \frac{p_0}{U_0} = \gamma$

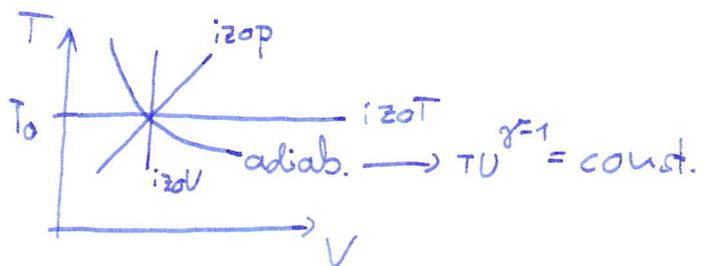
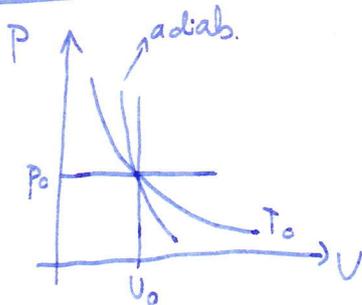
γ . szorososa
 (és $\gamma > 1$)

i) izoV, $V = \text{all.} \rightarrow dV = 0$
 $\delta W = 0$

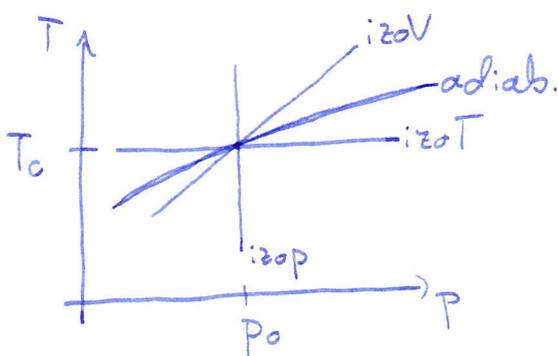


$Q = U_2 - U_1 = n C_V (T_2 - T_1)$

T2/1



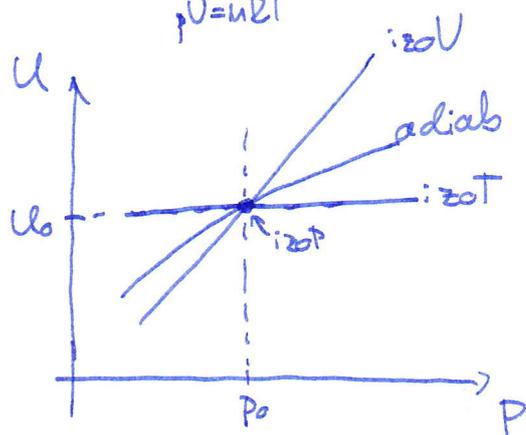
id. gáz: $pU = nRT \quad T = \frac{pU}{nR}$



T2/2

$$U = \frac{f}{2} k_B T = \frac{f}{2} k_B \frac{pV}{n}$$

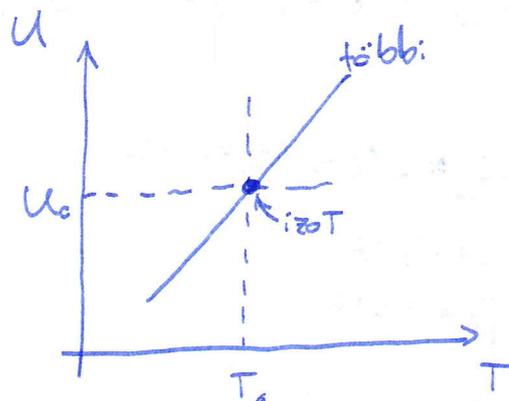
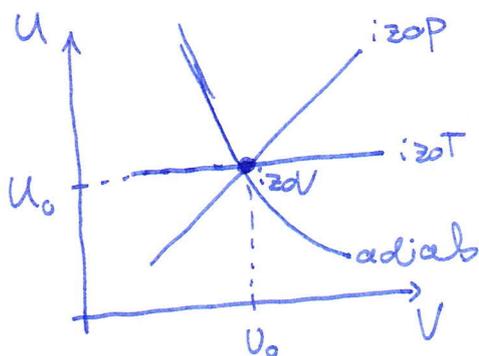
$$pV = nRT$$



$$pU^\gamma = \text{const}$$

$$\hookrightarrow pU = \text{const} \cdot U^{1-\gamma}$$

$$\text{const } p^{1-\frac{1}{\gamma}} \propto U$$



T2/3

p = all.

γ ismert

$$\Delta W \propto \Delta Q \propto \Delta U$$

$$\gamma = \frac{c_p}{c_v} = \frac{f+2}{f} \rightarrow f\gamma = f+2$$

$$f(\gamma-1) = 2$$

$$\Rightarrow f = \frac{2}{\gamma-1} \Rightarrow \frac{f}{2} = \frac{1}{\gamma-1}$$

$$\Delta W_{\frac{f}{2}} = p \Delta V = nR \Delta T \rightarrow \Delta T = \frac{\Delta W}{nR}$$

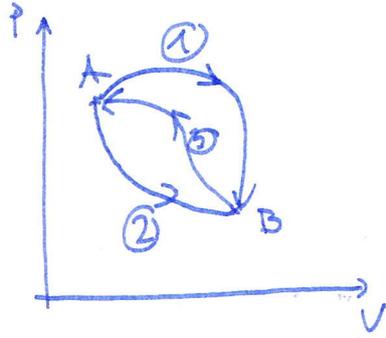
$$\Delta U = \frac{f}{2} nR \Delta T = \frac{f}{2} \Delta W \Rightarrow \Delta U = \frac{1}{\gamma-1} \Delta W$$

$$\Delta Q = c_p n \Delta T = c_p \frac{\Delta W}{R} \quad c_v = \frac{1}{n} \left. \frac{\partial U}{\partial T} \right|_v = \frac{f}{2} R \quad c_p - c_v = R$$

$$c_p = c_v + R = \frac{f}{2} R + R = R \left(\frac{f}{2} + 1 \right) = \gamma c_v = R \left(1 + \frac{1}{\gamma-1} \right) = R \frac{\gamma}{\gamma-1}$$

$$\Delta Q = \Delta W \frac{\gamma}{\gamma-1} = \gamma \Delta U$$

T2/4



$$\Delta Q_1 = 100 \text{ J}$$

$$\Delta W_{1,8} = 30 \text{ J}$$

$$\Delta Q_2 = ?$$

$$a, \Delta W_{2,8} = 10 \text{ J}$$

$$b, \Delta Q_3 = ?$$

$$\Delta W = 20 \text{ J}$$

ΔU folgt über 1, 2, 3 eselben u.a., irány ± 1

$$\Delta U = \Delta W_{in} + \Delta Q = \Delta Q - \Delta W_{out} = \underline{70 \text{ J}} = \Delta U_{1,2,3}$$

$$a) \Delta Q_2 = \Delta U + \Delta W_{out} = 80 \text{ J}$$

$$b, \Delta U = -70 \text{ J}$$

$$\Delta W_{out} = -20 \text{ J}$$

$$\Delta Q_3 = -80 \text{ J}$$

T2/5

$$\kappa_T = \frac{1}{\beta}$$

Kompress.

$$K = -\frac{1}{V} \left. \frac{\partial U}{\partial p} \right|_{\text{allpotuallt.}}$$

$$\kappa_{ad} = \frac{1}{\gamma p}$$

högg κ \oplus leggen norm. utgagabur

$$U(p) = \frac{N k_B T}{p}$$

$$\left. \frac{\partial U}{\partial p} \right|_T = -N k_B T / p^2 = -\frac{U}{p}$$

$$\kappa_T = \frac{1}{\beta}$$

$$\text{adiab} \Rightarrow pV^\gamma = \text{const} \quad / \cdot \frac{d}{dV}$$

$$\left(\frac{d}{dp} \right)$$

$$\frac{\partial}{\partial V} V^\gamma + p \gamma V^{\gamma-1} = 0$$

$$\hookrightarrow \frac{dp}{dV} = -\frac{\gamma p}{V} \Rightarrow \frac{dU}{dP} = -\frac{U}{\gamma p} \rightsquigarrow \kappa_{ad} = \frac{1}{\gamma p}$$

$$\kappa_{ad} = \frac{1}{\gamma p}$$

T2/6

$p = p(T, V) \checkmark$
 $\beta_p, \kappa_T \checkmark$

$c = \frac{1}{u} \frac{dQ}{dT}$

$\kappa_T = -\frac{1}{V} \frac{\partial V}{\partial p} \Big|_T$

$\beta_T = \frac{1}{V} \frac{\partial V}{\partial T} \Big|_p$

$\frac{\partial p}{\partial T} \Big|_V = ?$

izop \Rightarrow

$dp=0 = \frac{\partial p}{\partial T} \Big|_V dT + \frac{\partial p}{\partial V} \Big|_T dV \quad / \frac{d}{dT}$

$0 = \frac{\partial p}{\partial T} \Big|_V \underbrace{\frac{\partial T}{\partial T}}_1 + \frac{\partial p}{\partial V} \Big|_T \underbrace{\frac{\partial V}{\partial T} \Big|_p}_{\frac{1}{\kappa_T} \times \beta_T}$

$\Rightarrow \frac{\partial p}{\partial T} \Big|_V = \frac{\beta_p}{\kappa_T}$

izou \Rightarrow

$dU=0 = \frac{\partial U}{\partial T} \Big|_p dT + \frac{\partial U}{\partial p} \Big|_T dp \quad / \frac{d}{dT}$

izot \Rightarrow

$dT=0 = \frac{\partial T}{\partial p} \Big|_V dp + \frac{\partial T}{\partial V} \Big|_p dV \quad / \frac{d}{dp}$

T2/7

$V, p_0, T_1 \rightarrow T_2$

$\Delta U = ?$

$pV = N \beta T = N k_B T = \text{const} \Rightarrow NT = \text{const}$

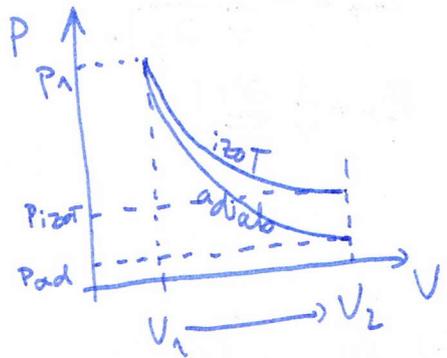
$N \sim \frac{\text{const}}{T}$

$U = \frac{f}{2} N k_B T = \frac{f}{2} k_B \cdot \text{const}$

$\Delta U = 0$

amennyivel nő az ~~be~~ energiája a bent lévő részecskéknél, pont annyi megy ki.

2/8
 U_1, γ
 ad, T
 $U_2 = ?$



izot: $p_1 U_1 = P_{2, izot} U_2$

ad: $p_1 U_1^\gamma = P_{2, ad} U_2^\gamma = \frac{P_{2, izot}}{2} U_2^\gamma$

feladat adja meg

$\frac{ad}{izot} \Rightarrow U_1^{\gamma-1} = \frac{1}{2} U_2^{\gamma-1} \rightarrow U_2 = U_1 2^{\frac{1}{\gamma-1}}$

Val. gázok: vdW

moln k.h. véges méret } korábban vettük őket

1 mol.

Mol. kiterj.:

mozgáshoz rendelt térfogat
 kevesebb, kisebb

$U \rightarrow U_M - b$
 ↓
 1 mol. ↑
 molék által elfoglalt

Nowais: Edlnak átadott i.e.p. csökken

$p \rightarrow p + p_{KH} =$ köhéziós nyomás

visszatérő mol.-ák számaival: } $p_{KH} \sim \frac{1}{U_M^2}$
 ütköző mol.-ák

$p_{KH} = \frac{a}{U_M^2}$

vdW: $(p + p_{KH})(U_M - b) = RT$

$(p + \frac{a}{U_M^2})(U_M - b) = RT \quad U_M = \frac{U}{M}$

n mol: $(p + \frac{n^2 a}{U^2})(U - nb) = nRT$

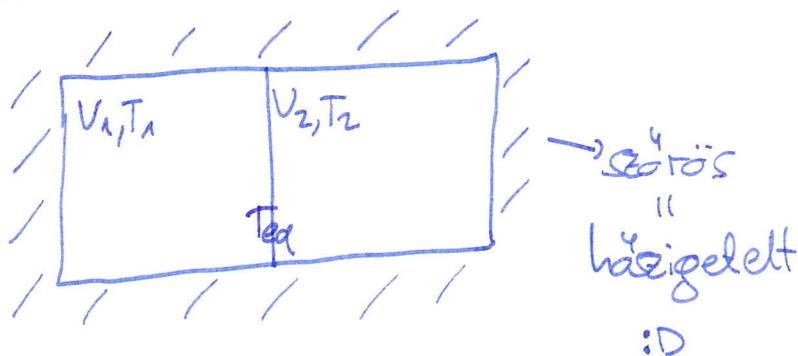
$$U_{kM} = \int_b^{U_M} P_{kM} dU'_M = \int_b^{U_M} \frac{a}{U_M^{1/2}} dU'_M = -\frac{a}{U_M} + \frac{a}{U_M} := \text{const}$$

$$U_k = \int_{b/v}^{V/v} \frac{u^2 a}{v^2} dV = -\frac{u^2 a}{V}$$

$$U_{\text{vold}} = U_{\text{id}} + U_k = \boxed{\frac{f}{2} nRT - \frac{u^2 a}{V}}$$

T2/3

$$U = C_V n T - \frac{u^2 a}{M^2 V}$$



a, $V_1, V_2 = \text{all.}$

$U = U_1 + U_2 = \text{all.}$

$$C_V n T_1 - \frac{u^2 a}{M^2 V_1} + C_V n T_2 - \frac{u^2 a}{M^2 V_2} = C_V T_{\text{eq}} n \cdot 2 - \frac{u^2 a}{M^2 V_1} - \frac{u^2 a}{M^2 V_2}$$

$$\boxed{T_{\text{eq}} = \frac{T_1 + T_2}{2}}$$

(10.05.)

Valód: gázok \sim UDL

\hookrightarrow k.h. figyelembevétele

\hookrightarrow korrekciók: $\left\{ \begin{array}{l} \text{véger kiterjedés} \\ \text{vonzás} \rightarrow \text{nyomás} \end{array} \right.$

1 mol V_M

$V_M \rightarrow V_M - b$ \rightarrow mol.-ák által kiszorított V

vonzás $p \rightarrow p + p_{ku}$

$\left. \begin{array}{l} \text{falsak ütköz} \text{ mol.-ák száma} \sim \frac{1}{V} \\ \text{visszaütköz} \text{ mol.-ák száma} \sim \frac{1}{V} \end{array} \right\} p_{ku} \sim \frac{1}{V^2} \sim \frac{1}{V_M^2}$

$p_{ku} = \frac{a}{V_M^2}$

$(p - p_{ku})(V - b) = \nu RT$

$(p + \frac{\nu^2 a}{V^2})(V - \nu b) = \nu RT$

$(p + \frac{a}{V_M^2})(V_M - b) = \nu RT$

$V_M = \frac{V}{\nu}$

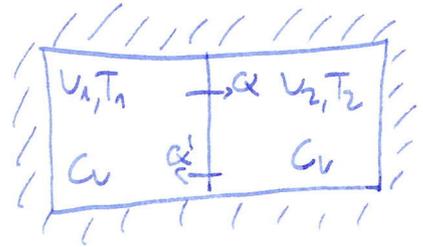
$U_{ku} = \int_b^{V_M} p_{ku} dV_M = a \int_b^{V_M} \frac{1}{V_M^2} dV_M = -\frac{a}{V_M} + \text{const} = 0 \rightarrow$ ez nem vezet jó mo.-ra \downarrow

$U_k = \int_{\frac{b}{\nu}}^{\frac{V}{\nu}} \frac{\nu^2 a}{V^2} \frac{dV}{\nu} = -\frac{\nu^2 a}{V} + \text{const}$

$U_{\text{val}} = U_{id} + U_a = \frac{f}{2} \nu RT - \frac{\nu^2 a}{V}$

T2/9

$$u = c_v m T - \frac{m^2}{M^2} \frac{a}{V}$$



a, $U_i = \text{const}$

$$u = u_1 + u_2 = \text{all.}$$

$$c_v m T_1 - \frac{m^2}{M^2} \frac{a}{V_1} + c_v m T_2 - \frac{m^2}{M^2} \frac{a}{V_2} =$$

$$= 2 c_v m T - \frac{m^2 a}{M^2 V_1} - \frac{m^2 a}{M^2 V_2}$$

$$T_{\text{eq}} = \frac{T_1 + T_2}{2}$$

b, lebontjuk a fázist

$$U_i \neq \text{const}$$

$$u = \text{const}$$

$$V = V_1 + V_2 = \text{const}$$

Zm gázunk lesz

$$c_v m T_1 - \frac{m^2}{M^2} \frac{a}{V_1} + c_v m T_2 - \frac{m^2}{M^2} \frac{a}{V_2} =$$

$$= 2 c_v T_{\text{eq}} - \frac{(2m)^2 a}{M^2 (V_1 + V_2)}$$

$$\Rightarrow T_{\text{eq}} = \frac{T_1 + T_2}{2} - \frac{m a}{2 M^2 c_v} \left(\frac{1}{V_1} + \frac{1}{V_2} - \frac{4}{V_1 + V_2} \right)$$

T2/10

$$U = U_0 (1 - a p + b T) \quad a, b = ?$$

$$\nu \rightarrow C, \beta_p, \kappa_T$$

$$a(p, T, \dots)$$

$$\left. \frac{\partial U}{\partial p} \right|_T = -U_0 a$$

$$\left. \frac{\partial U}{\partial T} \right|_p = U_0 b$$

$$\kappa_T = -\frac{1}{U_0} \left. \frac{\partial U}{\partial p} \right|_T \Rightarrow a = \kappa_T$$

$$\beta_p = \frac{1}{U_0} \left. \frac{\partial U}{\partial T} \right|_p \Rightarrow b = \beta_p$$

$$\Rightarrow U = U_0 (1 - \kappa_T p + \beta_p T)$$

T2/11

$$\beta_p = \frac{3aT^3}{U} \quad \kappa_T = \frac{b}{U} \quad a, b = \text{const.} : U$$

$$\beta_p = \frac{1}{U} \left. \frac{\partial U}{\partial T} \right|_p = \frac{3aT^3}{U} \rightarrow \left. \frac{\partial U}{\partial T} \right|_p = 3aT^3 \int \frac{1}{U} dT$$

$$U(p, T) = \frac{3}{4} a T^4 + f(p)$$

$$\left. \frac{\partial U}{\partial p} \right|_T = -b = \frac{df(p)}{dp} \quad // dp$$

$$f(p) = -bp + U_0 \quad \rightarrow \text{scale konst.}$$

$$U(p, T) = \frac{3}{4} a T^4 - bp + U_0$$

T2/12

$$[C_p - C_v](T, U, V, p) \quad \text{I. f. ö. l.} \quad \delta Q = dU + p dV$$

$$U = c_v n T - \frac{n^2 a}{V}$$

$$dU = \left. \frac{\partial U}{\partial T} \right|_V dT + \left. \frac{\partial U}{\partial V} \right|_T dV$$

$$\delta Q = \left[\left. \frac{\partial U}{\partial V} \right|_T + p \right] dV + \left. \frac{\partial U}{\partial T} \right|_V dT \quad // \frac{d}{dT} \left[\frac{1}{n} \frac{d\delta Q}{dT} \right]$$

$$C_p - C_v = \frac{1}{n} \left[\left. \frac{\partial U}{\partial V} \right|_T + p \right] \left. \frac{\partial U}{\partial T} \right|_V$$

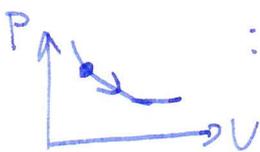
$$C_p - C_v = \frac{1}{n} \left[\frac{n^2 a}{V^2} + p \right] U V p$$

$$\rightarrow \left. \frac{\partial U}{\partial V} \right|_T = \frac{n^2 a}{V^2}$$

$$\left(p + \frac{n^2 a}{V^2} \right) (U - nb) = nRT$$

$$C_p - C_v = \frac{U V p}{n} = \frac{nRT}{U - nb}$$

\sim állapotváltozás



$$: \text{isothermal } \Delta T = 0$$

$$pV = nRT = \text{all.}$$

$$U(T) = \text{all}$$

$$\Delta U = 0 = n c_v \Delta T \Rightarrow$$

$$\Delta Q = -\Delta W_{\text{mi}} \rightarrow \text{mi végzett}$$

$$W_{\text{mi}} = - \int_{V_1}^{V_2} p dV = -nRT \int_{V_1}^{V_2} \frac{dV}{V} = -nRT \ln \frac{V_2}{V_1}$$

$$\Delta Q_{\text{fel}} = nRT \ln \frac{V_2}{V_1}$$

$$W_g = nRT \ln \frac{V_2}{V_1}$$

izov: $dU=0 \Rightarrow \boxed{W=0}$

$\Delta U = \Delta Q$

$\Delta Q = U_2 - U_1 = c_{v,m}(T_2 - T_1) = \frac{c_v}{\nu} U_1 (p_2 - p_1) = \Delta U$

izop: $p = \text{const.}$

$\Delta W_{\text{mech}} = -p(U_2 - U_1) = p(U_1 - U_2)$

$\Delta Q = U_2 - U_1 + p(U_2 - U_1) = n c_p \Delta T$

$\Delta U = n c_v \Delta T$

$\Delta W_{\text{mech}} = p(U_1 - U_2)$

$\Delta Q = p \frac{c_p}{\nu} (U_2 - U_1)$

$\Delta U = p \frac{c_v}{\nu} (U_2 - U_1)$

adiab: $\delta Q = 0 \Rightarrow \Delta Q = 0$

$\Delta W = \Delta U$

$pU^\gamma = \text{const} := k \rightarrow p_i = \frac{k_i}{U_i^\gamma}$

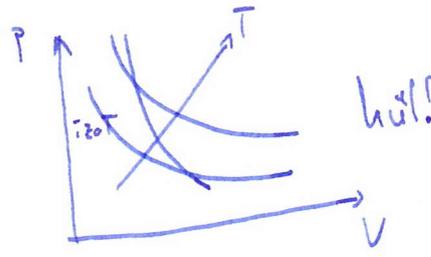
$W_{\text{mech}} = - \int_{U_1}^{U_2} p dU = - \int_{U_1}^{U_2} \frac{k_i}{U_i^\gamma} dU = - \frac{k_2 U_2^{1-\gamma} - k_1 U_1^{1-\gamma}}{1-\gamma}$

$W_{\text{mech}} = - \frac{p_2 U_2 - p_1 U_1}{\gamma - 1}$

δQ	ΔQ	ΔU	ΔW_{mech}
$p = \text{const}$	$p_1 \frac{c_p}{\nu} (U_2 - U_1)$	$p_1 \frac{c_v}{\nu} (U_2 - U_1)$	$p_1 (U_1 - U_2)$
$U = \text{const}$	$V_1 \frac{c_v}{\nu} (p_2 - p_1)$	$U_1 \frac{c_v}{\nu} (p_2 - p_1)$	0
$T = \text{const}$	$nRT \ln \frac{U_2}{U_1}$	0	$-nRT \ln \frac{U_2}{U_1}$
$\delta Q = 0$	0	$-\frac{p_1 U_1 - p_2 U_2}{\gamma - 1}$	$-\frac{p_1 U_1 - p_2 U_2}{\gamma - 1}$

T3/1

1 mol id. gáz $U = \frac{k}{\sqrt{p}}$ - mődon vált: jűb a
 $\sim p = \frac{k^2}{U^2}$



$c = ?$
 $c = \frac{1}{n} \frac{\delta Q}{dT}$
 $\delta Q = dU + p dV$
 $\begin{cases} \delta Q = n c dT \\ dU = n c_v dT \end{cases}$

$$dU = \left. \frac{\partial U}{\partial V} \right|_T dV + \left. \frac{\partial U}{\partial T} \right|_V dT$$

$$\delta Q = \left. \frac{\partial U}{\partial T} \right|_V dT + \left[\left. \frac{\partial U}{\partial V} \right|_T + p \right] dV$$

$$n c dT = n c_v dT + \left[\left. \frac{\partial U}{\partial V} \right|_T + p \right] dV$$

id.g. $\left. \frac{\partial U}{\partial V} \right|_T = 0$

$$n c dT = n c_v dT + p dV \rightarrow n c dT = \left[n c_v + p \left. \frac{dV}{dT} \right|_? \right] \cdot dT$$

$$pV = nRT \sim U = \frac{nRT}{p}$$

$$U = \frac{k}{\sqrt{p}} \quad p = \frac{k^2}{U^2}$$

$$U = \frac{nRT}{k^2} U^2 \quad \boxed{U = \frac{k^2}{nRT}}$$

$$\frac{dU}{dT} = -\frac{k^2}{nRT^2} = -\frac{U}{T}$$

$$c_v dT = c_v \frac{dU}{dT} dT - \frac{p}{T} dT$$

$$\hookrightarrow \frac{nRT}{T}$$

$$\boxed{C = C_v - R}$$

T3/2

$c = \text{all. } c_p, c_v, U$

előzetes: $n c dT = \left[n c_v + p \left. \frac{dV}{dT} \right|_{\text{ad.}} \right] dT$

$$c n dT = c_v n dT + \frac{nRT}{V} \left. \frac{dV}{dT} \right|_{\text{ad.}} dT$$

$$\frac{c - c_v}{R} \frac{dT}{T} = \frac{dV}{V} \quad / \int$$

$$\frac{c - c_v}{R} \ln T = \ln V + \ln k$$

$$T = k \cdot V^{\frac{R}{c - c_v}} \cdot \frac{pV}{nR} = T$$

$$\frac{c - c_v}{R} \ln \frac{pV}{nR} = \ln V + \ln k$$

$$p = k' V^{\frac{R}{c - c_v} - 1} \quad nR = k' \cdot V^{\frac{R}{c - c_v} - 1} = k' U^{\frac{c_p - c_v}{c - c_v}}$$

T3/3



$$p = A(v)$$

$$c(v) = C_v + R \frac{f(v)}{f(v) + v \frac{df}{dv}}$$

$$c(v) = C_v + R \frac{f(v)}{f(v) + v \frac{df}{dv}}$$

jó-e erre előző feladat?

$$p = \frac{k^2}{v^2}$$

$$\frac{dp}{dv} = -\frac{2k^2}{v^3}$$

$$\Rightarrow c = C_v + R \frac{\frac{k^2}{v^2}}{\frac{k^2}{v^2} - v \frac{2k^2}{v^3}} = C_v - R$$

Teljesít c...re jó

→ korábbi öi

$$c = C_v + \frac{1}{n} p \frac{dv}{dT} \Big|_{\text{á.v.}}$$

$$f(v)v = pV = nRT \rightarrow T = \frac{f(v)v}{nR}$$

$$\frac{dT}{dv} = \left(\frac{dv}{dT} \right)^{-1} \quad \frac{dT}{dv} = \frac{1}{nR} \left(v f'(v) + f(v) \right)$$

$$\frac{dv}{dT} \Big|_{\text{á.v.}} = \frac{nR}{v \cdot f'(v) + f(v)}$$

$$c = C_v + \frac{f(v)}{n} \frac{nR}{\frac{df}{dv} v + f(v)}$$

$$c(v) = C_v + R \frac{f(v)}{f(v) + v \frac{df}{dv}}$$

□

(10.12.)

$$c(v) = c_v + \frac{f(v)R}{\frac{df}{dv}v + f(v)} \quad \text{Istfall}$$

b, P_m, U_m

$$p = a - bV \quad \text{d.v.}$$

$T = \text{max}$

$$\left. \begin{aligned} pU &= nRT \\ f''(v)U & \end{aligned} \right\}$$

$$\left. \frac{\partial T}{\partial v} \right|_{U_m} = 0 = \frac{a - 2bU}{nR} \Rightarrow \boxed{U_m = \frac{a}{2b}}$$

$$T(v) = \frac{pU}{nR} = \frac{f(v)U}{nR} = \frac{(a - bV)U}{nR}$$

$$P_m = p(U_m) = a - b \frac{a}{2b} = \boxed{\frac{a}{2}}$$

$$\boxed{T^{3/2}} \quad c(v) = c_v + \frac{f(v)R}{\frac{df}{dv}v + f(v)} = \text{const}$$

$$c(v) = c_v + \frac{R}{1 + \frac{v}{p} \frac{dp}{dv}} = \text{const}$$

$\underbrace{\frac{v}{p} \frac{dp}{dv}}_{\text{const} := \lambda} \quad \frac{v}{p} \frac{dp}{dv} = \lambda$

$$\frac{dp}{p} = \lambda \frac{dv}{v} \quad | \cdot \int$$

$$\ln \frac{p}{p_0} = \lambda \ln \frac{v}{v_0}$$

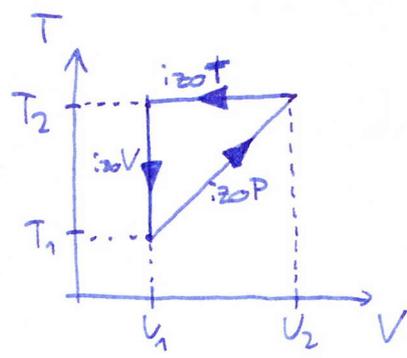
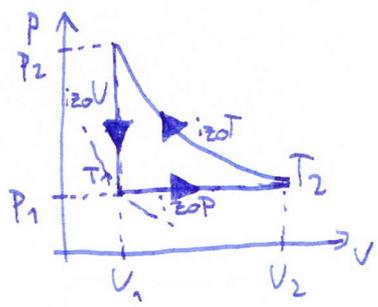
$$\boxed{p = p_0 \left(\frac{v}{v_0} \right)^\lambda}$$

$$c(v) = c_v + \frac{R}{1 + \lambda}$$

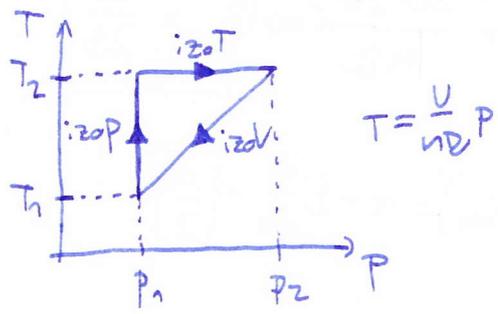
$$\lambda = \frac{R}{c - c_v} - 1 = \frac{c_p - c}{c - c_v}$$

$$\boxed{p = p_0 \left(\frac{v}{v_0} \right)^{\frac{c_p - c}{c - c_v}}}$$

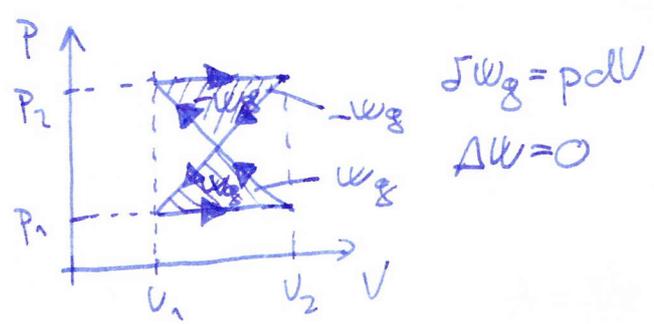
T3/4-5



$$T = \frac{P}{nR} V$$



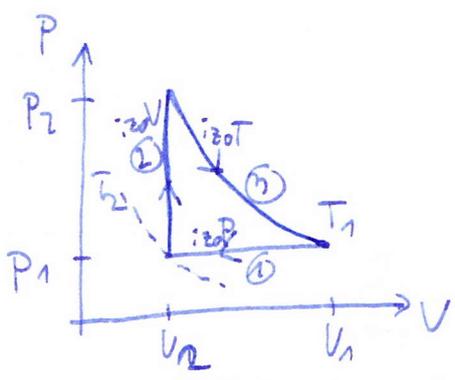
$$T = \frac{V}{nR} P$$



$$\int \delta W_g = p dV$$

$$\Delta U = 0$$

T3/6



a, $\Delta U_1 = ?$ a, $\Delta U_1 = \frac{f}{2} nR(T_2 - T_1) = \frac{f}{2} P_1 (V_2 - V_1) = \frac{P_1 (V_2 - V_1)}{\gamma - 1}$

b, $\Delta Q_2 = ?$

c, $\Delta W_g, \Delta Q_2 = ?$

b,

① $dU = 0 \quad \Delta U_2 = 0$

$\Delta U_2 = \Delta Q_2$

$\Delta U_2 - \Delta U_1 = \Delta Q_2$

c, $\Delta U = \oint dU = 0 \quad \oint \delta Q = \oint \delta W = \Delta W_1 + \Delta W_2 + \Delta W_3 = P_1 (V_2 - V_1) + P_1 V_1 \ln \frac{V_1}{V_2}$

$\Delta W_1 = P_1 (V_2 - V_1)$

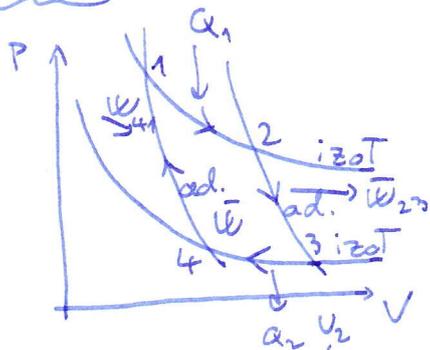
$\Delta W_2 = 0$

$\Delta W_3 = \int_{V_2}^{V_1} p dV = nRT_1 \int_{V_2}^{V_1} \frac{1}{V} dV = nRT_1 \ln \frac{V_1}{V_2} = nR \frac{P_1 V_1}{nR} \ln \frac{V_1}{V_2}$

HATA'S FOL

Reverzibilis Carnot

$dU=0$



1 mol id.g.

$\bar{w} \Rightarrow$ gáz végzi

$w \Rightarrow$ mi végzünk

1-2: $Q_{12} = Q_1 = -W_{12} = \int_{V_1}^{V_2} p(V) dV = RT_1 \ln \frac{V_2}{V_1} > 0$ hőfelv. $Q_{be} = Q_{fd}$

2-3: $Q_{23} = 0$ $W_{23} = U_3 - U_2 = C_V (T_3 - T_2)$
 $\downarrow < 0 \Rightarrow \bar{w}_{23} > 0$

3-4: $Q_{34} = Q_2 = -W_{34} = RT_2 \ln \frac{V_4}{V_3} < 0$ hőlead. ($-Q_2 = Q_{le} = Q_{ki}$)

4-1: $Q_{41} = 0$

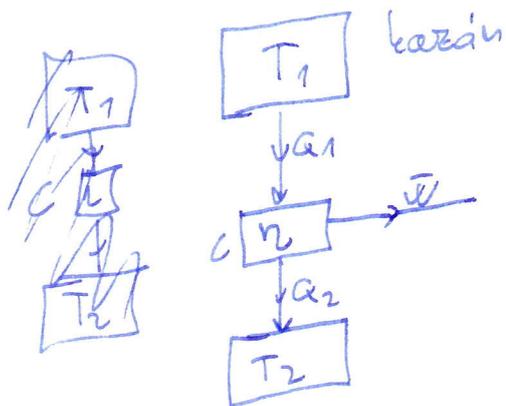
$W_{41} = C_V (T_2 - T_3) > 0$

$\bar{w} = - (W_{12} + W_{23} + W_{34} + W_{41})$

$\bar{w} = RT_1 \ln \frac{V_2}{V_1} + RT_2 \ln \frac{V_4}{V_3} > 0$

$\bar{w} = Q_1 + Q_2$

\Downarrow gáz hőfelv. árán munkát végez



$\eta := \frac{\bar{w}}{Q_1} = \frac{\bar{w}_{gáz}}{Q_{fel}} \leq \frac{Q_1 + Q_2}{Q_1} = 1 + \frac{Q_2}{Q_1}$

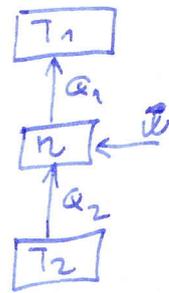
$\frac{Q_2}{Q_1} = \frac{RT_2 \ln \frac{V_4}{V_3}}{RT_1 \ln \frac{V_2}{V_1}} = -\frac{T_2}{T_1} \Rightarrow \frac{Q_1}{T_1} + \frac{Q_2}{T_2} = 0$
 red. hő

$\eta_c = 1 - \frac{T_2}{T_1} = 1 - \frac{T_{kisebb}}{T_{nagyobb}} = \eta_c$

$Q = \frac{Q_1}{T_1} + \frac{Q_2}{T_2}$

II. f. t. (Planck)
 $\eta < 1$

hőszivattyú / hűtő gép



Teljesítménytényező:

$$k_{h.s.} = \frac{|Q_1^f|}{W} = \frac{1}{\eta} \quad Q_1^f = -Q_1$$

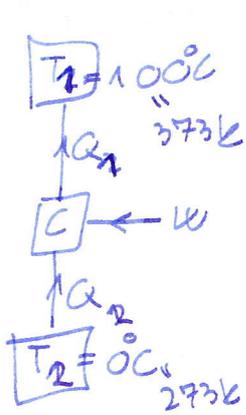
$$k_{h.g.} = \frac{Q_2}{W} = \frac{T_2}{T_1 - T_2}$$

általánosán:

$$\eta = 1 - \frac{Q_{le}}{Q_{fel}} = 1 + \frac{Q_2}{Q_1}$$

Csapat: fgtl. az anyagi minőségtől

T3/7



$$L_f = 2,25 \cdot 10^6 \frac{J}{kg}$$

$$m_g = 1 kg \text{ gőz}$$

$$L_o = 3,35 \cdot 10^5 \frac{J}{kg}$$

$$W = ?$$

$$\eta_c = 1 - \frac{T_2}{T_1}$$

$$\eta = \frac{\Delta W}{Q_1} = \frac{Q_1 - |Q_2|}{Q_1} = 1 - \frac{|Q_2|}{Q_1}$$

$$\Rightarrow \frac{|Q_2|}{Q_1} = \frac{T_2}{T_1}$$

$$Q_1 = L_f \cdot m_g$$

$$Q_2 = L_o \cdot m_j$$

$$\frac{|Q_2|}{Q_1} = \frac{T_2}{T_1} = \frac{L_o m_j}{L_f m_g} \Rightarrow m_j = \frac{T_2 L_f m_g}{T_1 L_o} =$$

$$\approx \boxed{4,32 kg}$$

! KELVIN!

$$\Delta W = \eta Q_1 = \left(1 - \frac{T_2}{T_1}\right) L_f m_g \approx \boxed{6036 J}$$

$$1 kWh = 3600 J$$

$$[W] = \left[\frac{J}{s}\right]$$

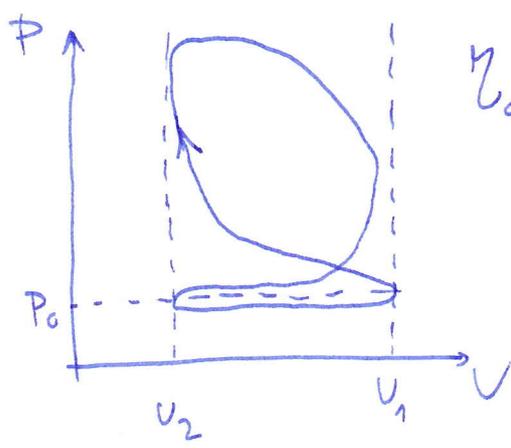
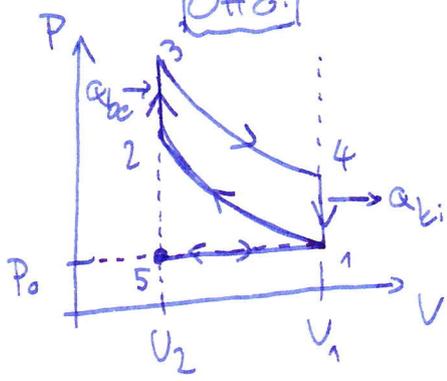
$$J = W \cdot s$$

$$Wh = 3600 Ws = 3600 J$$

$$1 kWh = 3600 kJ$$

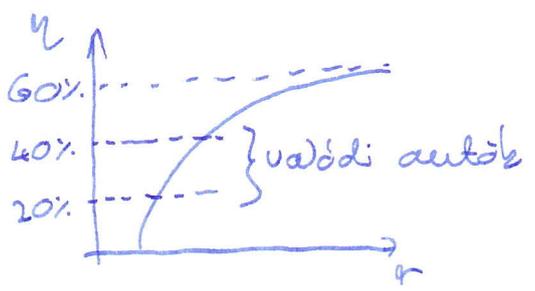
9 Ft

Otto:

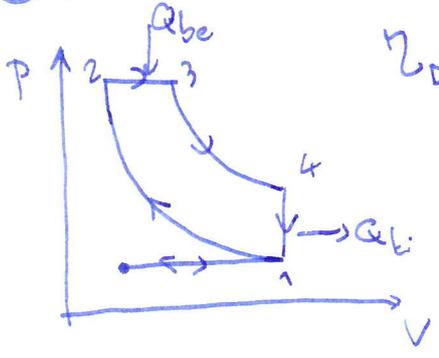


$$\eta_o = 1 - \frac{1}{(V_1/V_2)^{\gamma-1}} = 1 - \frac{1}{r^{\gamma-1}}$$

angagi parameter =>
=> obtained



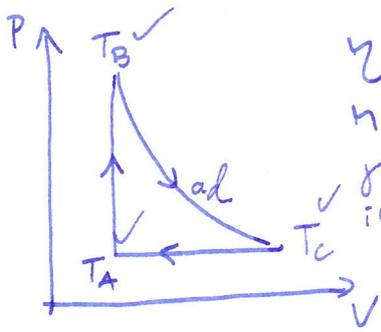
DIESEL:



$$\eta_D = 1 - \frac{T_1}{\gamma T_2} \frac{(T_4/T_1 - 1)}{(T_3/T_2 - 1)}$$

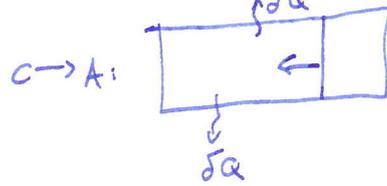
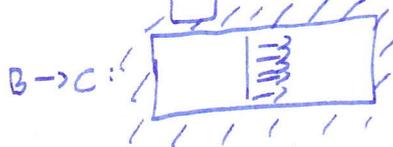
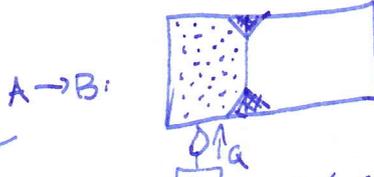
(10.19.)

T3/8



$\eta = ?$
 $n = 1 \text{ mol}$
 γ
 id.g.

$$\eta = \frac{W}{Q_{\text{fel}}} = \frac{Q_{\text{fel}} - |Q_{\text{lel}}|}{Q_{\text{fel}}} = 1 - \frac{|Q_{\text{lel}}|}{Q_{\text{fel}}}$$



$$|Q_{\text{lel}}| = n c_p (T_C - T_A)$$

$$Q_{\text{fel}} = n c_v (T_B - T_A)$$

$$\frac{c_p}{c_v} = \gamma \Rightarrow \eta = 1 - \gamma \frac{T_C - T_A}{T_B - T_A}$$

$$T_C \Rightarrow T_C V_C^{\gamma-1} = T_B V_B^{\gamma-1} \rightarrow T_C = T_B \left(\frac{V_B}{V_C} \right)^{\gamma-1}$$

$$= T_B \left(\frac{T_A}{T_C} \right)^{\gamma-1}$$

$$\frac{V_B}{V_C} = \frac{T_A}{T_C}$$

$$\Rightarrow T_C = \left(\frac{T_B T_A}{T_C} \right)^{\frac{1}{\gamma}}$$

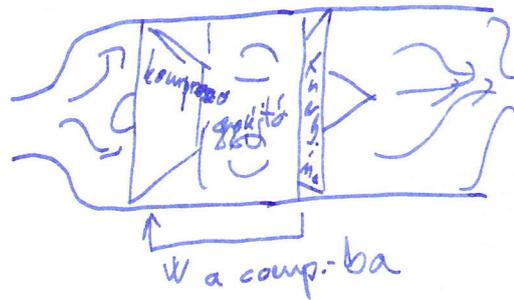
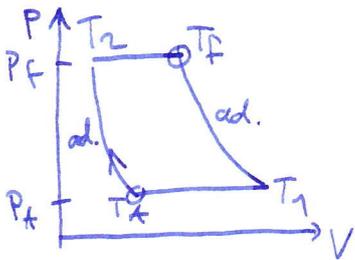
$$\eta = 1 - \gamma \frac{\left(\frac{T_B T_A}{T_C} \right)^{\frac{1}{\gamma}} - T_A}{T_B - T_A}$$

T3/9

n mol, id.g.

$\eta = ?$
 $\eta(f) = ?$
 max $\eta = ?$

Soule ciklus
 Brayton - n -



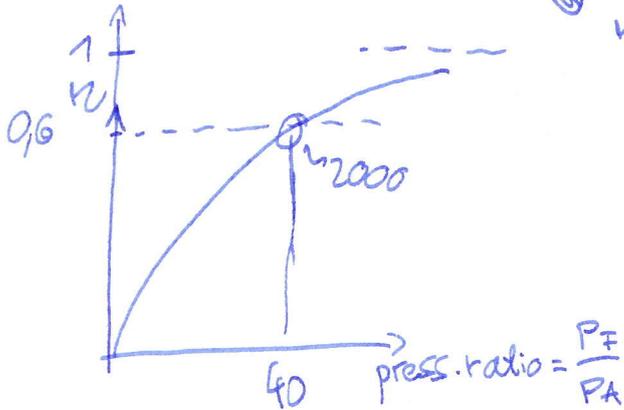
$$\eta = 1 - \frac{|Q_{\text{lel}}|}{Q_{\text{fel}}} = 1 - \frac{c_p (T_C - T_A)}{c_p (T_B - T_2)}$$

$T_1, T_2 = ?$

$$TV^{\gamma-1} = \text{const} \rightarrow p_A^{\frac{1-\gamma}{\gamma}} T = \text{const} \quad \frac{T_1}{T_2} = \left(\frac{p_A}{p_F}\right)^{\frac{1-\gamma}{\gamma}} := x \quad \frac{T_2}{T_1} = \frac{1}{x}$$

$$\Rightarrow \eta = 1 - \frac{T_F x - T_A}{T_F - T_A/x} = 1 - x = 1 - \left(\frac{p_A}{p_F}\right)^{\frac{1-\gamma}{\gamma}}$$

$$\gamma = \frac{f+2}{f} \rightarrow \frac{1-\gamma}{\gamma} = \frac{2}{2+f} \quad \frac{p_A}{p_F} < 1$$

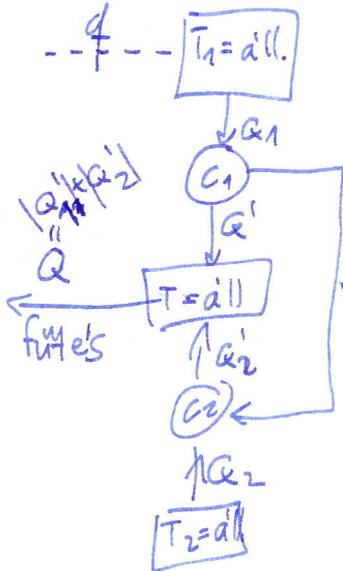


$\eta \uparrow \Leftrightarrow f \downarrow$

úgy kapunk maxot, ha egy atomos $f=3$ gáz veszi, illetve $\eta \uparrow \Leftrightarrow \frac{p_A}{p_F} \downarrow$

T3/10

$$T_1 > T_2 > T_3 \quad T_1 > T > T_2 \quad \eta_1 = \frac{W}{Q_1} = 1 - \frac{|Q_2|}{Q_1} = 1 - \frac{|Q_1'|}{Q_1} = 1 - \frac{T}{T_1}$$



$$Q_1 = q$$

$$W = Q_1 - |Q_1'| = Q_1 \left(1 - \frac{T}{T_1}\right)$$

$$|Q_1'| = Q_1 \frac{T}{T_1}$$

$$\eta_2 = 1 - \frac{T_2}{T} = \frac{W}{|Q_2'|} \quad |Q_2'| = \frac{W}{1 - \frac{T_2}{T}} = \frac{Q_1 \left(1 - \frac{T}{T_1}\right)}{1 - \frac{T_2}{T}}$$

$$Q = |Q_1'| + |Q_2'| = \dots = Q_1 \frac{1 - \frac{T_2}{T}}{1 - \frac{T}{T_1}}$$

$$Q = Q_1 \frac{1 - \frac{T_2}{T}}{1 - \frac{T}{T_1}} > q$$

$$T_2 < T < T_1$$

$$\frac{T_2}{T_1} < \frac{T}{T}$$

↓ ZH IDÁIG

II. Főtétel

Clausius: \nexists olyan folyamat amely pusztán abból állna, hogy a hő a hidegebb helyről a melegebb felé áramlik

$\Rightarrow \exists$ olyan foly.-ok, amelyek az E megm.-nak megfelelő mérséklet mellett végbemennek.

Entropia: "rendezetlenség mértéke" \Rightarrow egyre több szabadsági fokra oszlik át az energia

I.F.T.: E megm. \Rightarrow mi lehet végre

II.F.T.: \Rightarrow mi fog végbemenni:

S : állapot függ., extenzív

rev. foly.: ved. hő = entropia megváltoz. - a hőfelv. $S \uparrow$
hőleadás $S \downarrow$

$$dS = \frac{dQ^{\text{rev.}}}{T} \quad //$$

$$S_A - S_B = \int_B^A \frac{dQ^{\text{rev.}}}{T} \quad \text{rev. körfoly.} \quad \boxed{dS=0} \quad \oint dS=0 = \oint \frac{dQ^{\text{rev.}}}{T}$$

irrev. foly.: $dS \geq 0$ entropia produkció

$$\oint \frac{dQ^{\text{irrev.}}}{T} < 0$$

$$\frac{dQ^{\text{irrev.}}}{T} < dS$$

$$\frac{dQ}{T} \leq dS$$

$$dS = \frac{dQ}{T} + dS_{\text{prod.}} = \frac{dQ}{T} + d\sigma$$

izolált r.sz., term. egyensúly $\Leftrightarrow S$ max. értéket
 $\leadsto dS=0$

$$\boxed{dS = \frac{\delta Q}{T} = \frac{dU - \delta W}{T} = \frac{C_V n dT}{T} + \frac{p dV}{T}}$$

$$\boxed{dU = T ds - p dV}$$

I. fundamentalis
eggenwet

$$pV = nRT \quad /:d$$

$$V dp + dV p = nR dT \quad /:T$$

$$\boxed{\frac{dp}{p} + \frac{dV}{V} = \frac{dT}{T}}$$

T4/1

$$p_1 = 2 \cdot 10^6 \text{ Pa}$$

$$T = 27^\circ \text{C} = \text{all.}$$

$$V_1 = 1 \text{ liter} = \text{all.}$$

idg

$$p_2 = 10^5 \text{ Pa}$$

$$\Delta S = ?$$

$$dS = \frac{\delta Q}{T}$$

$$T dS = \delta Q = C_V n dT + \frac{nRT}{V} dV \rightarrow dS = C_V n \frac{dT}{T} + nR \frac{dV}{V}$$

$$\delta Q = dU + p dV$$

$$C_V n dT \quad \downarrow \quad p = \frac{nRT}{V}$$

$$\boxed{\Delta S = S_2 - S_1 = C_V n \ln \frac{T_2}{T_1} + nR \ln \frac{V_2}{V_1}}$$

isot \rightarrow

isot

$$\underline{\underline{\Delta S = nR \ln \frac{V_2}{V_1}}} \iff V_i = \frac{nRT}{p_i}$$

$$\Delta S = nR \ln \frac{p_1}{p_2} ; \quad n = \frac{p_1 V_1}{RT}$$

$$\boxed{\Delta S = \frac{p_1 V_1}{RT} \ln \frac{p_1}{p_2}} \approx 20 \frac{\text{J}}{\text{K}}$$

T4/2 $m=1g$ $V_2 \Rightarrow f=5$
 $\Delta S=?$
 $i z o P \Rightarrow P = \text{const.}$
 $V_1 = 1 \text{ liter}$
 $V_2 = 5 \text{ liter}$

$P = P_1 = P_2$
 $T_i = \frac{P}{nR} V_i$
 $\frac{T_2}{T_1} = \frac{V_2}{V_1}$

$dS = n c_v \frac{dT}{T} + nR \frac{dV}{V}$

$S_2 - S_1 = n c_v \ln \frac{T_2}{T_1} + nR \ln \frac{V_2}{V_1} = \underbrace{(n c_v + nR)}_{n c_p} \ln \frac{V_2}{V_1} = n c_p \ln \frac{V_2}{V_1} = 3,34 \frac{J}{K}$

$\left. \begin{matrix} \frac{c_p}{c_v} = \gamma \sim f \\ c_p - c_v = R \end{matrix} \right\} c_p = \frac{f+2}{2} R = \frac{7}{2} R$ $m \Rightarrow n$ $M_{U_2} = \frac{1}{4} \frac{g}{mol}$

T4/3 $m, M, \gamma, idg.$

a, $S(T, V) = ?$

b, \downarrow ad $dQ = 0 \Leftrightarrow dS = 0 \Rightarrow S = S_0$

$c_p - c_v = R$
 $c_p = R + c_v = \gamma c_v$
 $c_v = \frac{R}{\gamma - 1}$

$dS = n c_v \frac{dT}{T} + nR \frac{dV}{V}$

$\int_{S_0}^{S} dS = 0$
 $\ln \left[\frac{T}{T_0} \right] = 0$
 $= 1$

$S = S_0 + nR \ln \left[\left(\frac{T}{T_0} \right)^{\frac{1}{\gamma-1}} \frac{V}{V_0} \right]$

$S - S_0 = n c_v \ln \frac{T}{T_0} + nR \ln \frac{V}{V_0}$

adiabata $\left(\frac{T}{T_0} \right)^{\frac{1}{\gamma-1}} \frac{V}{V_0} = 1$

T4/4 $S(T, V) = n c_v \ln T + nR \ln V + S_0$

a, $S_0(n)$ extensiv $dU = int * d(ext)$

b, $S_0(n) = ?$

$S = \sum S_i = n \bar{S}$ $\bar{S}_i = \frac{1}{n} \sum S_i$
 it'reerse.

$S(T, V, n) = n \left(c_v \ln T + R \ln \frac{V}{V_n} + R \ln \frac{V}{V_n} + \frac{S_0(n)}{n} \right) = n \left(c_v \ln T + R \ln V + S_0 \right)$

$S_0(n) = -nR \ln n + n S_0$

$T V^{\gamma-1} = const$

T4/5

(10.26.)

$m = 1 \text{ kg}$

$T_0 = 0^\circ\text{C} \rightarrow T_1 = 100^\circ\text{C}$: izop
vize

273K

373K

$\Delta S = ?$

$dS = \frac{dQ}{T}$

melegítés $\Delta S_1 = \int_{T_0}^{T_1} \frac{dQ}{T} = cm \int_{T_0}^{T_1} \frac{dT}{T} = cm \ln \frac{T_1}{T_0}$
 $dQ = cm dT$

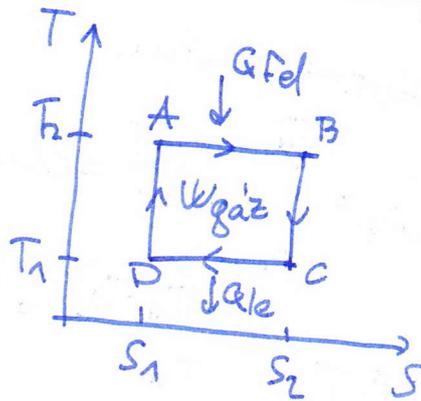
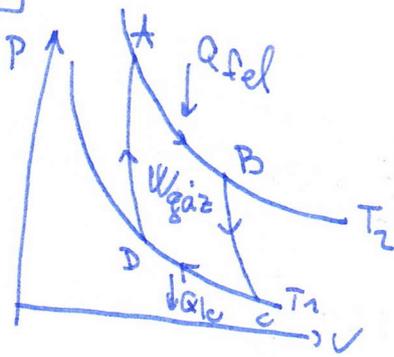
$c = 4.18 \frac{\text{kJ}}{\text{kgK}}$

gőzölés $\Delta S_2 = \int \frac{dQ}{T} = \frac{L_f m}{T_1}$

$\Delta S = \Delta S_1 + \Delta S_2$

$dQ = L_f m$

T4/7



ad: $dQ = 0 \rightarrow dS = 0$

$dQ = du + pdv$

$\oint dQ = \oint du + \oint pdv$

$dS = \frac{dQ}{T} \Rightarrow dQ = T dS$

körfoly. $\oint du = 0$

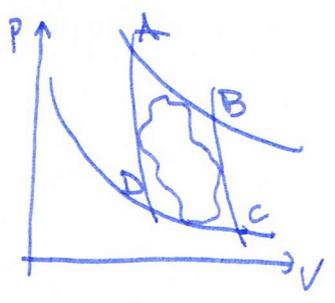
$\oint T dS = \oint pdv$
 W_{gaz}

$= 1 - \frac{|Q_{le}|}{Q_{fel}} = 1 - \frac{T_1 \Delta S}{T_2 \Delta S} = 1 - \frac{T_1}{T_2}$

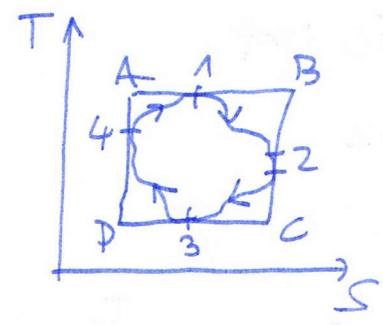
KörT...

$$\eta = 1 - \frac{|Q_c|}{Q_h}$$

mutatis:



=>



$$\int_4^1 T ds + \int_1^2 T ds > 0 \text{ hőfelv.}$$

→ hő hőm. ⇒ hő S

$$\int_2^3 T ds + \int_3^4 T ds < 0 \text{ hőleadás}$$

← hő csök. ⇒ S csök.

T4/6 $m = 1 \text{ kg}$

$T_0 = 273 \text{ K}$ víz

$T_H = 373 \text{ K}$ hőforr. → all. hőm.

a, $dS = \frac{dQ}{T}$ $\Delta S_{\text{víz}} = \int_{T_0}^{T_H} cm \frac{dT}{T} = cm \ln \frac{T_H}{T_0} = \boxed{1306 \frac{\text{J}}{\text{K}}}$

b, $\Delta S_{\text{tart.}} = \frac{\Delta Q}{T_H} = \frac{-cm(T_H - T_0)}{T_H} = \boxed{-1121 \frac{\text{J}}{\text{K}}}$
hőleadás

c) tejes ΔS entrópia változás

$$\Delta S = \Delta S_{\text{víz}} + \Delta S_{\text{tart.}} = cm \left[\ln \left(\frac{T_H}{T_0} \right) + \frac{T_0}{T_H} - 1 \right] = \boxed{185 \frac{\text{J}}{\text{K}}} > 0$$

d) $T_i = 323 \text{ K}$ ⇒ $\Delta S_{\text{víz}} = \int_{T_0}^{T_i} \frac{dQ}{T} + \int_{T_i}^{T_H} \frac{dQ}{T} = \left(\int_{T_0}^{T_i} + \int_{T_i}^{T_H} \right) \frac{dQ}{T} = \int_{T_0}^{T_H} \frac{dQ}{T} = cm \ln \frac{T_H}{T_0}$

$\Delta S_{\text{tart.}}^{(1)} = \frac{\Delta Q^{(1)}}{T_i} = \frac{-cm(T_i - T_0)}{T_i}$

$\Delta S_{\text{tart.}}^{(2)} = \frac{\Delta Q^{(2)}}{T_H} = \frac{-cm(T_H - T_i)}{T_H}$

$\Delta S'_{\text{tart.}} = cm \left(\frac{T_0}{T_i} + \frac{T_i}{T_H} - 2 \right) = \boxed{-1208 \frac{\text{J}}{\text{K}}}$
hővesztés → $\Delta S' = \boxed{98 \frac{\text{J}}{\text{K}}}$

$$\Delta S_{\text{start}}' = c_m \left(\frac{T_0}{T_H} - 1 - \left[1 + \frac{T_0}{T_H} - \frac{T_0}{T_i} - \frac{T_i}{T_H} \right] \right) = \Delta S_{\text{start}} - c_m \left[1 + \frac{T_0}{T_H} - \frac{T_0}{T_i} - \frac{T_i}{T_H} \right]$$

$$\frac{\partial \Delta S_{\text{start}}'}{\partial T_i} \Big|_{\text{min}} = 0 = \left[+ \frac{T_0}{T_i^2} - \frac{1}{T_H} \right] (c_m)$$

$$\frac{T_0}{T_i^2} = \frac{1}{T_H} \rightarrow T_i^* = \sqrt{T_0 T_H}$$

e, N tartals
 $\Delta T = \frac{T_H - T_0}{N}$, $N \rightarrow \infty$, $\Delta T \rightarrow 0$

$$\Delta S_{\text{viz}} = \int_{T_0}^{T_H} \frac{\delta Q}{T} = c_m \ln \frac{T_H}{T_0}$$

$$\Delta S_{\text{tot}}'' = - \lim_{N \rightarrow \infty} (c_m \left[\frac{\Delta T}{T_1} + \frac{\Delta T}{T_2} + \dots + \frac{\Delta T}{T_N} \right]) = - c_m \lim_{N \rightarrow \infty} \sum_{i=1}^N \frac{\Delta T}{T_i} =$$

$$\int_{T_0}^{T_H} \frac{dT}{T} \text{ ha } N \rightarrow \infty; \Delta T \rightarrow 0$$

$$= - c_m \int_{T_0}^{T_H} \frac{dT}{T} = - \Delta S_{\text{viz}} \quad \Delta S_{\text{tot}} = 0$$

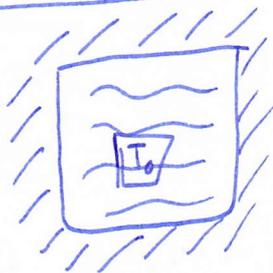
T4/9

$$\left. \begin{aligned} m_1 &= 0,2 \text{ kg} \\ T_1 &= 373 \text{ K} \end{aligned} \right\} \text{Fe}$$

$$\left. \begin{aligned} m_2 &= 0,5 \text{ kg} \\ T_2 &= 285 \text{ K} \end{aligned} \right\} \text{H}_2\text{O}$$

$$c_1 = 0,46 \frac{\text{J}}{\text{gK}}$$

$$c_2 = 4,18 \frac{\text{J}}{\text{gK}}$$



$$c_1 m_1 (T_1 - T_k) = c_2 m_2 (T_k - T_2)$$

$$c_1 m_1 T_1 - c_1 m_1 T_k = c_2 m_2 T_k - c_2 m_2 T_2$$

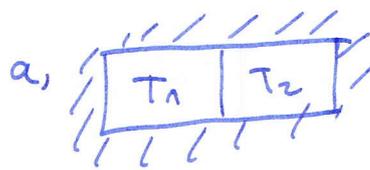
$$c_1 m_1 T_1 + c_2 m_2 T_2 = T_k (c_1 m_1 + c_2 m_2)$$

$$T_k = \frac{c_1 m_1 T_1 + c_2 m_2 T_2}{c_1 m_1 + c_2 m_2} = \underline{\underline{288,7 \text{ K}}}$$

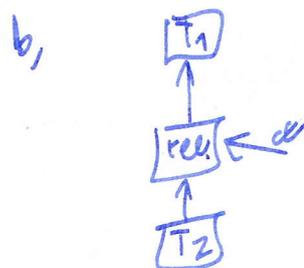
$$\Delta S = \Delta S_{\text{Fe}} + \Delta S_{\text{H}_2\text{O}} = \int_{T_1}^{T_k} \frac{c_1 m_1}{T} dT + \int_{T_2}^{T_k} \frac{c_2 m_2}{T} dT =$$

$$= c_1 m_1 \ln \frac{T_k}{T_1} + c_2 m_2 \ln \frac{T_k}{T_2} = 3,41 \frac{\text{J}}{\text{K}}$$

T4/10 $c = 100 \frac{J}{K}$
 $T_1 = 273K$
 $T_2 = 373K$



$T_k = ?$
 $T'_k = ?$
 $\Delta U_b = \Delta U_{b,1} + \Delta U_{b,2} =$
 $= c(T'_k - T_1) + c(T'_k - T_2) =$
 $= 2c\left(\sqrt{T_1 T_2} - \frac{T_1 + T_2}{2}\right) \leq 0$



a) $c(T_k - T_1) = c(T_2 - T_k)$

$T_k = \frac{cT_1 + cT_2}{2c} = \frac{T_1 + T_2}{2}$

$c, \Delta U_i = ?$
 $\Delta S_i = ?$
 $\Delta U = 0$

b, rev. $\Delta S = 0$

$dS = \frac{dQ}{T}$ $dQ = dU - \delta W_{vis} = dU + p dV$ $dU = c_v dT$

$dS = c_v \frac{dT}{T} + \frac{p dV}{T}$

$dU = 0$

$\Delta S_i = c_v \ln \frac{T_i^{(neg)}}{T_i^{(pos)}}$
 $i = 1, 2$
 $\frac{T_1}{T_2}$

$\Delta S = 0 = \Delta S_1 + \Delta S_2 = \phi \ln \frac{T'_k}{T_1} + \phi \ln \frac{T'_k}{T_2} =$
 $= \phi \ln \frac{T_k'^2}{T_1 T_2}$
 $T'_k = \sqrt{T_1 T_2}$

a, $\Delta U_a = 0 = \Delta U_{a,1} + \Delta U_{a,2} \Rightarrow \Delta U_{a,1} = -\Delta U_{a,2}$ $\Delta U_{a,1} = c_v(T_k - T_1) =$
 $= c_v\left(\frac{T_1 + T_2}{2} - T_1\right) = c_v\left(\frac{T_2 - T_1}{2}\right)$

$\Delta S_a = \Delta S_{a,1} + \Delta S_{a,2}$

$\Delta S_{a,1} = \int \frac{dQ}{T} = c_v \int_{T_1}^{T_2} \frac{dT}{T} = c_v \ln \frac{T_2}{T_1}$

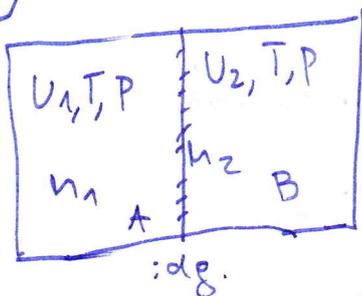
$\Delta S_{a,2} = c_v \ln \frac{T_k}{T_2}$

$\Delta S_a = c_v \ln \frac{T_k^2}{T_1 T_2} =$
 $= 2c_v \ln \frac{T_k}{\sqrt{T_1 T_2}} =$

$= 2c_v \ln \frac{\frac{T_1 + T_2}{2}}{\sqrt{T_1 T_2}} \Rightarrow 0$

(11.02.)

T4/8



- a) Biz. $T, P \neq \text{vált}$
- b) $\Delta S = ?$
- c) ΔS , ha $A = B$

jel: $i=1,2$ tart.
 A, B gáz

kezdi: $pU_1 = n_1 RT_1; n_1 = n_A$
 $pU_2 = n_2 RT_2; n_2 = n_B$

Tell, mert izolált rendszer

a) Dalton-tv.

$$P_A = \frac{n_A k_B T}{V_1 + V_2}$$

$$P_B = \frac{n_B k_B T}{V_1 + V_2}$$

$$P^* = P_A + P_B = \frac{n_A k_B T + n_B k_B T}{V_1 + V_2} = \frac{pU_1 + pU_2}{V_1 + V_2} = p$$

$$b) dS = c_v n \frac{dT}{T} + \frac{pdU}{T} \stackrel{p = \frac{nRT}{U}}{\downarrow} = c_v n \frac{dT}{T} + \frac{nRT}{T} \frac{dU}{U}$$

$$\Delta S_j = c_v n_j \ln \frac{T_j^{\text{vég}}}{T_j^{\text{kez}} + n_j R \ln \frac{U_j^{\text{vég}}}{U_j^{\text{kez}}}$$

$$\left. \begin{aligned} U_A^{\text{kez}} &= U_1 \\ U_B^{\text{kez}} &= U_2 \end{aligned} \right| \begin{aligned} U_A^{\text{vég}} &= U_B^{\text{vég}} \\ &= U_1 + U_2 \end{aligned}$$

$$\Delta S = \Delta S_A + \Delta S_B = R \left(n_A \ln \frac{U_1 + U_2}{U_1} + n_B \ln \frac{U_1 + U_2}{U_2} \right) = R \left(n_A \ln \frac{n_A + n_B}{n_A} + n_B \ln \frac{n_A + n_B}{n_B} \right)$$

$$U_1 = \frac{n_A RT}{P} \quad U_2 = \frac{n_B RT}{P}$$

$$n_A = n_1 \\ n_B = n_2$$

azaz nem hiányos $\Delta S \geq 0$

c) $\Delta S = 0$ nagyon sok a részecske, gyakorlatilag mindig, hogy ott van-e a fal, vagy sem

Gibbs-paradoxon

Gibbs-paradoxon:

Boltzmann: $S = k_B \ln W$

W : adott makroáll. hoz tartozó mikroáll.-ok száma

legyen 2 golyó, piros, kék
vagy 2g. m. mikro

1.	2.	} túlszámolás.
p	p	
p	k	
k	p	
k	k	
m		Ha 1. 2. nem
4 mikroáll.		kül., akkor
		pk u.a. min
		kp mégis
		2x vetlen

$W_{kezd} = W_1 \cdot W_2$

$W_{veg} =$

$\Delta S = k_B \ln \frac{W_{veg}}{W_{kezd}} = k_B \ln \frac{W_{veg}}{W_1 W_2}$

$\Delta S = k_B \left(\ln \left(\frac{N_A + N_B}{N_A} \right)^{N_A} + \ln \left(\frac{N_A + N_B}{N_B} \right)^{N_B} \right)$

$S^* = k_B \ln W^* = k_B \ln \frac{W}{\prod_j N_j!}$ megkül.-telen

\Rightarrow T4/8 $\Delta S^* = k_B \ln \frac{W_{veg}^*}{W_{kezd}^*} = k_B \ln \left(\frac{W_{veg}}{W_{kezd}} \cdot \frac{N_A! N_B!}{(N_A + N_B)!} \right) = \Delta S$

azonos gázok: $\Delta S^* = k_B \ln \left(\frac{W_{veg}}{W_{kezd}} \cdot \frac{N_A! N_B!}{(N_A + N_B)!} \right)$

↳ nem tudjuk melyik hovan jött

Stirling-formula:

$$\ln N! \approx N \ln N - N$$

$$\Delta S^* = \Delta S(\dots) = k_B \ln 1 = 0$$

$$N_A \ln \frac{N_A}{N_A + N_B} + N_B \ln \frac{N_B}{N_A + N_B}$$

↑
u.o. gázok keverése

ha nem u.o. gázok keverése, és $p = \text{const}$ $T = \text{const}$, akkor is változik az S , mert több lesz a mikroállapotok száma \Rightarrow keveredési entropia

FUNDAMENTÁLIS ESEMENYEK

kémiai pot., Maxwell-tel.

Kémiai pot.

1 részecske kivételéhez szükséges energia: $\mu \rightarrow$ intenzív
kontinuum anyag
ext. párja: N
1 mol kivételéhez....

I. Fund. eqg: $du = Tds - pdv + \mu dn \rightsquigarrow U(S, V, N) = ?$

$$\mu = \left. \frac{\partial U}{\partial N} \right|_{S, V}$$

U extenzív
↓

Több komponens: $\sum_i \mu_i dn_i$

$$dU = \underbrace{\left. \frac{\partial U}{\partial S} \right|_{V, N}}_T ds + \underbrace{\left. \frac{\partial U}{\partial V} \right|_{S, N}}_{-P} dv + \underbrace{\left. \frac{\partial U}{\partial N} \right|_{S, V}}_{\mu} dn$$

Euler-egyenlet:

U.: $U(S, V, N)$ homogén, elsőrendű fgv.-e
a változóinak

homogén



$$U(\lambda S, \lambda V, \lambda N) = \lambda U(S, V, N) \quad / \frac{d}{d\lambda}$$

↳ extenzív, elsőrendű, nincs olyan, hogy
pl. 2-tösszeadok és 3x-es lesz

$$\frac{dU}{d\lambda} = \frac{\partial U}{\partial \lambda S} \frac{\partial \lambda S}{\partial \lambda} + \frac{\partial U}{\partial \lambda V} \frac{\partial \lambda V}{\partial \lambda} + \frac{\partial U}{\partial \lambda N} \frac{\partial \lambda N}{\partial \lambda} = U(S, V, N)$$

$\underbrace{\quad\quad\quad}_{T} \quad \underbrace{\quad\quad\quad}_{S} \quad \underbrace{\quad\quad\quad}_{-P} \quad \underbrace{\quad\quad\quad}_{V} \quad \underbrace{\quad\quad\quad}_{\mu} \quad \underbrace{\quad\quad\quad}_{N}$

$$\frac{\partial U}{\partial S} = \frac{\partial \lambda U}{\partial \lambda S}$$

$\underbrace{\quad}_{T} \quad \underbrace{\quad}_{T}$

$$U(S, V, N) = TS - pV + \mu N$$

$$dU = TdS + \underbrace{SdT - pdV - Vdp + \mu dN + d\mu N}_{\text{int. menny.-ek diff.-jai}}$$

Gibbs-Duhem rel.

$$SdT - Vdp + Nd\mu = 0$$

$$\hookrightarrow d\mu = -\frac{S}{N}dT + \frac{V}{N}dp$$

összefüggés \Rightarrow
 \Rightarrow pusztán integrálással
nem lehet kélni
a r.a.-t, kell min.
1 extenzív is

ξ_i : ext., X_i : int.

$$U(\xi_i) = \sum_i X_i \xi_i$$
$$dU(\xi_i) = \sum_i X_i d\xi_i$$

:D kanonikusan konjugált :D

} kis-kanonikus sokaság

Legendre-trafo. $\rightarrow d(\text{int})$

Helmholtz szabadenergia: $F = U - TS$ } kanonikus sokaság

$$dF = dU - TdS - SdT = \cancel{TdS} - pdU + \mu dU - \cancel{TdS} - SdT =$$

$$= -SdT - pdU + \mu dU = dF$$

Entalpia: $H = U + pV$

$$dH = dU + dpV + pdV = TdS + Vdp + \mu dU$$

Gibbs: $G = H - TS$

$$dG = dH - TdS - SdT = -SdT + Vdp + \mu dU$$

Termodin.-i pot.: $\phi = U - TS - \mu U$

$$d\phi = -SdT - pdV - Udp$$

} Nagykanonikus sokaság

T5/1

$$dU = TdS - pdU + \mu dN$$

$$\left. \frac{\partial U}{\partial S} \right|_{V, N} = T$$

$$\left. \frac{\partial U}{\partial V} \right|_{S, N} = -P$$

$$\left. \frac{\partial U}{\partial N} \right|_{V, S} = \mu$$

$$dF = -SdT - pdU + \mu dN$$

$$\left. \frac{\partial F}{\partial T} \right|_{V, N} = -S$$

$$\left. \frac{\partial F}{\partial V} \right|_{T, N} = -P$$

$$\left. \frac{\partial F}{\partial N} \right|_{T, V} = \mu$$

$$dG = -SdT + Vdp + \mu dN$$

$$\left. \frac{\partial H}{\partial S} \right|_{P, N} = T$$

$$\left. \frac{\partial H}{\partial P} \right|_{S, N} = V$$

$$\left. \frac{\partial H}{\partial N} \right|_{S, P} = \mu$$

$$dG = -SdT + Vdp + \mu dN$$

$$\left. \frac{\partial G}{\partial T} \right|_{P, N} = -S$$

$$\left. \frac{\partial G}{\partial P} \right|_{T, N} = V$$

$$\left. \frac{\partial G}{\partial N} \right|_{T, P} = \mu$$

T5/8

$$pV = A(T) + B(T)p + C(T)p^2 \rightarrow V = \frac{A}{P} + B + Cp$$

T fix, $p_0 \rightarrow p_1$

$\Delta G, \Delta S = ?$

$$\left. \frac{\partial G}{\partial P} \right|_{T, N} = V = \frac{A}{P} + B + Cp$$

$$\int_{p_0}^{p_1}$$

$$\Delta G = ? \quad \Delta G = A(T) \ln \frac{p_1}{p_0} + B(T)(p_1 - p_0) + \frac{C(T)}{2}(p_1^2 - p_0^2)$$

T5/1

$$-\Delta S = \frac{\partial G}{\partial T} \Big|_{P,U}$$

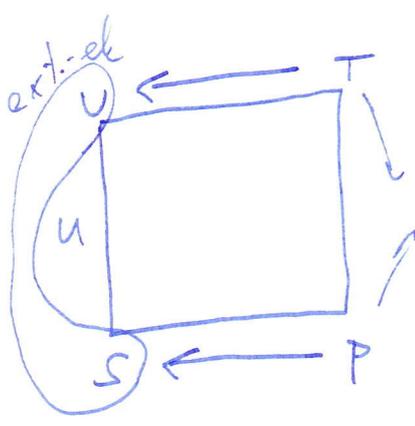
$$\Delta S = \frac{dK(T)}{dT} \ln \left(\frac{P_0}{P_1} \right) + \frac{dB(T)}{dT} (P_0 - P_1) + \frac{dC(T)}{dT} (P_0^2 - P_1^2)$$

T5/2

Mx-rel. \Leftrightarrow Young-tétel a Fund.e-re

$$dU = TdS - PdV + \mu dN = \frac{\partial U}{\partial S} \Big|_{U,N} dS + \frac{\partial U}{\partial V} \Big|_{S,N} dV - \left(\frac{\partial U}{\partial N} \Big|_{S,U} dN \right)$$

$$\frac{\partial}{\partial V} \frac{\partial U}{\partial S} \Big|_V = \frac{\partial}{\partial S} \frac{\partial U}{\partial V} \Big|_S \Rightarrow \boxed{\frac{\partial T}{\partial V} \Big|_S = \frac{\partial P}{\partial S} \Big|_V}$$



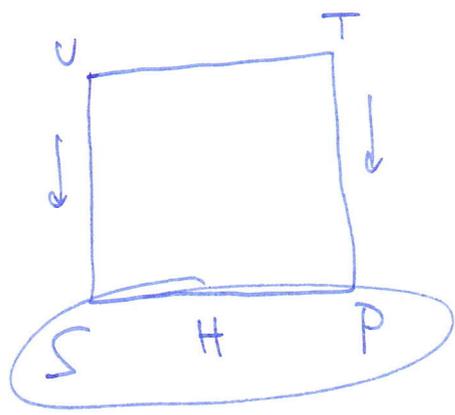
ezekkel az int.-ekkel

- vízszintes nyílak $\times (-1)$
- függőleges nyílak $\times (+1)$
- ferde nyílak $\times (\mp \gamma)$

$$dH = TdS + VdP$$

$$\frac{\partial}{\partial P} \frac{\partial H}{\partial S} \Big|_P = \frac{\partial}{\partial S} \frac{\partial H}{\partial P} \Big|_S$$

$$\boxed{\frac{\partial T}{\partial P} \Big|_S = \frac{\partial V}{\partial S} \Big|_P}$$



T5/1

$$dF = -SdT - pdv$$

$$\frac{\partial}{\partial v} \frac{\partial F}{\partial T} \Big|_v = \frac{\partial}{\partial T} \frac{\partial F}{\partial v} \Big|_T$$

$\underbrace{\quad}_{-S} \qquad \underbrace{\quad}_{-P}$

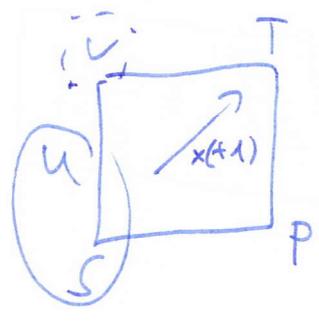
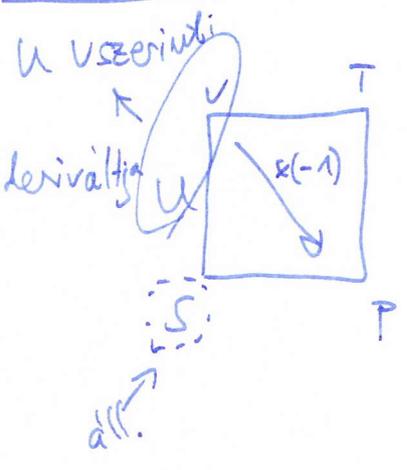
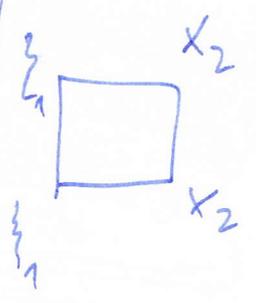
$$\frac{\partial S}{\partial v} \Big|_T = \frac{\partial P}{\partial T} \Big|_v$$

$$dG = -SdT + Vdp \quad (\mu dN)$$

$$\frac{\partial}{\partial p} \frac{\partial G}{\partial T} \Big|_p = \frac{\partial}{\partial T} \frac{\partial G}{\partial p} \Big|_T$$

$\underbrace{\quad}_{-S} \qquad \underbrace{\quad}_V$

$$-\frac{\partial S}{\partial p} \Big|_T = \frac{\partial V}{\partial T} \Big|_p$$



(11.03.)

T5/3

$dU=0$ $\frac{\partial U}{\partial U}|_T = T \frac{\partial p}{\partial T} - p$ $dU = \frac{\partial U}{\partial U}|_T dU + \frac{\partial U}{\partial T}|_U dT = dTS - p dU$ / "dU|T"

$\frac{\partial U}{\partial U}|_T = T \frac{\partial S}{\partial U}|_T - p \Rightarrow \frac{\partial U}{\partial U}|_T = T \frac{\partial p}{\partial T}|_U - p$

es soll, ist es oder ateg: ist uen

-p → x
U → z

$dU = \sum_i X_i dx_i = T ds + X dz$ / : dz|T

$\frac{\partial U}{\partial z}|_T = T \frac{\partial S}{\partial z}|_T + X$

$dU = \frac{\partial U}{\partial S}|_z dS + \frac{\partial U}{\partial z}|_S dz$

$\frac{\partial S}{\partial z}|_T = - \frac{\partial X}{\partial T}|_z$

$\frac{\partial}{\partial z} = \frac{\partial}{\partial S}$

$\frac{\partial U}{\partial z}|_T = -T \frac{\partial X}{\partial T}|_z + X$

$T ds = dU^{(T,S)} - X dz$
 $ds = \frac{1}{T} \frac{\partial U}{\partial T}|_z dT - \frac{1}{T} \left(\frac{\partial U}{\partial z}|_T - X \right) dz$

$\frac{\partial^2 S}{\partial T \partial z} = \frac{\partial^2 S}{\partial z \partial T}$

Young tétel nem csak a potenciállovánál, hanem a Maxwell egyenletek szintjén is.

$\frac{\partial}{\partial z} \left(\frac{1}{T} \frac{\partial U}{\partial T}|_z \right) = \frac{\partial}{\partial T} \left(\frac{1}{T} \frac{\partial U}{\partial z}|_T - \frac{X}{T} \right)$

T5/5

$S = S(p, T)$ $T ds = n c_p dT - \beta p T V dp$

$c_p = \frac{\partial H}{\partial T}|_p$ $c_v = \frac{\partial U}{\partial T}|_V$ $\beta p = \frac{1}{V} \frac{\partial V}{\partial T}|_p$ $\beta p = - \frac{1}{V} \frac{\partial V}{\partial p}|_T \leftrightarrow \beta p = - \frac{1}{V} \frac{\partial U}{\partial p}|_S$

$ds = \frac{\partial S}{\partial p}|_T dp + \frac{\partial S}{\partial T}|_p dT$

$\frac{\partial S}{\partial T}|_p \Rightarrow \frac{\partial S}{\partial T}|_p \cdot \frac{\partial H}{\partial H}|_p = n c_p \frac{\partial S}{\partial H}|_p$

$\frac{1}{T} n c_p$
 $\frac{\partial S}{\partial H}|_p = \frac{\partial H}{\partial S} = T$
 $dH = dU + p dV + V dp$

$-\frac{\partial V}{\partial T}|_p = -V \beta p$

$T ds = n c_p dT - V \beta p T dp$

kis. Fiz. 3. Gy. - 5

FÁZISÁTVÁLTSÓK

jel: $G \rightarrow \text{mel} \quad N \rightarrow n \quad (1 \text{ molra nézve } \theta - t)$

fázis \Rightarrow gáz, foly., szilárd stb. \leadsto anyag homogén részét

komponens \Rightarrow anyagok: Mgtl

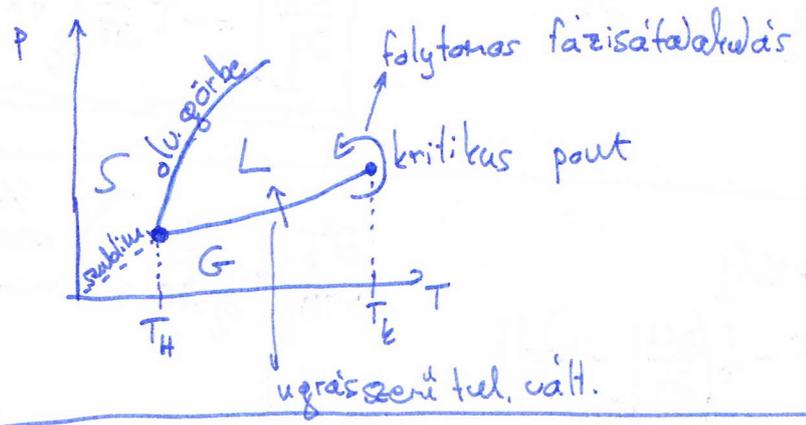
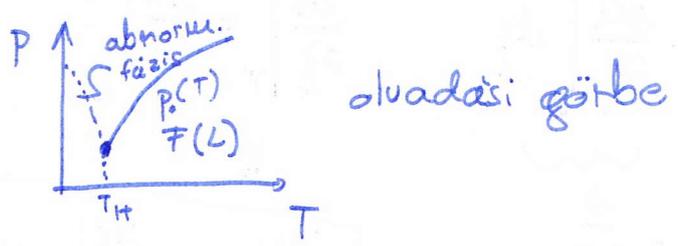
↓
fázishatár zárja le

fázishatáron áthaladva ugrásszerűen változhatnak a tul.ók

TÁPASETALAT: olvadás során T nem vált.

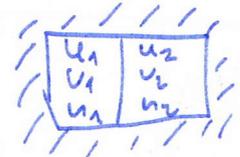
\hookrightarrow betáplált energia a ned. kötérséget szelvéja fel

\Rightarrow pot. \uparrow ; ΦT



Fázisegyensúly feltétele:

a, izolált r.sz.
 $U = U_1 + U_2$
 $V = V_1 + V_2$
 $n = n_1 + n_2$



$dS = 0$ \Rightarrow haem nő tovább \rightarrow egyensúly

$$S = S_1(U_1, V_1, n_1) + S_2(U_2, V_2, n_2)$$

$$U_2 = U - U_1$$

...

$$0 = dS(\underbrace{U, V, n}_{\text{paraméterek}}, \underbrace{U_1, V_1, n_1}_{\text{változók}}) = \left[\frac{\partial S_1}{\partial U_1} \Big|_{V_1, n_1} - \frac{\partial S_2}{\partial U_2} \Big|_{V_2, n_2} \right] dU_1 + \left[\frac{\partial S_1}{\partial V_1} \Big|_{U_1, n_1} - \frac{\partial S_2}{\partial V_2} \Big|_{U_2, n_2} \right] dV_1 + \dots$$

$dU_2 = -dU_1$

$$\dots + \left[\frac{\partial S_1}{\partial n_1} \Big|_{u_1, n_1} - \frac{\partial S_2}{\partial n_2} \Big|_{u_2, n_2} \right] dn_1 = 0$$

$$\sum_i x_i = 0; x_i \geq 0$$

$$\Downarrow$$

$$\forall x_i = 0$$

$$\frac{\partial S_1}{\partial u_1} \Big|_{u_1, n_1} = \frac{\partial S_2}{\partial u_2} \Big|_{u_2, n_2} \quad \frac{\partial S}{\partial u} \Big|_{u, n} = \frac{1}{T}$$

$$\frac{\partial S_1}{\partial v_1} \Big|_{u_1, n_1} = \frac{\partial S_2}{\partial v_2} \Big|_{u_2, n_2} \quad \frac{\partial S}{\partial v} \Big|_{u, n} = \frac{p}{T}$$

$$\frac{\partial S}{\partial n} \Big|_{u, v} = - \frac{\mu}{T}$$

$\Rightarrow \begin{cases} T_1 = T_2 \\ p_1 = p_2 \\ \mu_1 = \mu_2 \end{cases} \Rightarrow$
 ind. menny.-ek
 egyenlőek
 \Downarrow
 egyenlőség
 "Secreti"
 $\mu(T, p)$

b, izoT-izop r.e.

$$\boxed{dG=0} \quad G(T, p, n_1) = G_1(T, p, n_1) + G_2(T, p, n_2)$$

$$n = n_1 + n_2$$

$$dn_2 = \cancel{dn_1} - dn_1$$

$$0 = dG = \left[\frac{\partial G_1}{\partial T} \Big|_{p, n_1} - \frac{\partial G_2}{\partial T} \Big|_{p, n_2} \right] dT + \left[\dots \right] dp + \boxed{\frac{\partial G_1}{\partial n_1} \Big|_{p, T} dn_1 + \frac{\partial G_2}{\partial n_2} \Big|_{p, T} dn_2}$$

$$0 = dG = \frac{\partial G_1}{\partial n_1} \Big|_{T, p} dn_1 + \frac{\partial G_2}{\partial n_2} \Big|_{T, p} dn_2$$

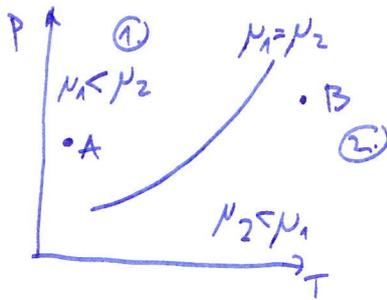
$$\left[\frac{\partial G_1}{\partial n_1} - \frac{\partial G_2}{\partial n_2} \right] dn_1$$

$$\boxed{\mu_1 = \mu_2}$$

Fázisdiagramm:

egyensúly: áll.-at leíró $p = f(T)$ fgv. ahol

$\mu_1 = \mu_2$

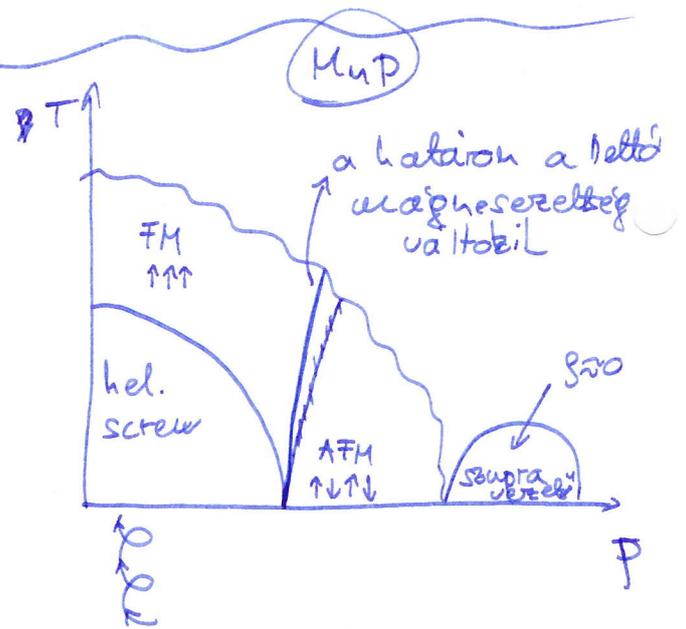
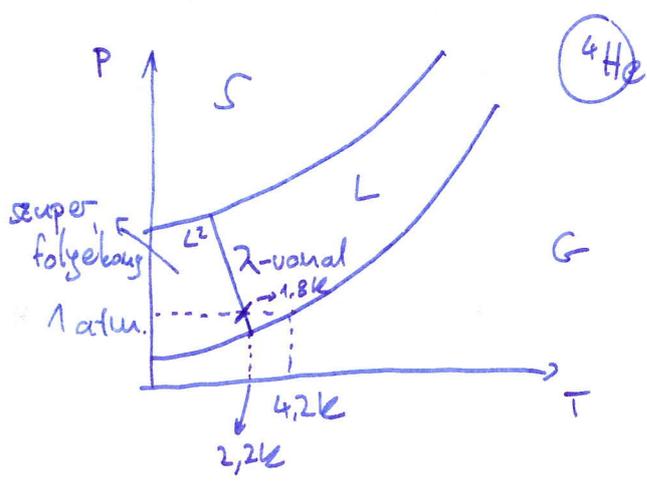


A-ban $\exists \text{ } \textcircled{2}$ (egyensúlytétel)

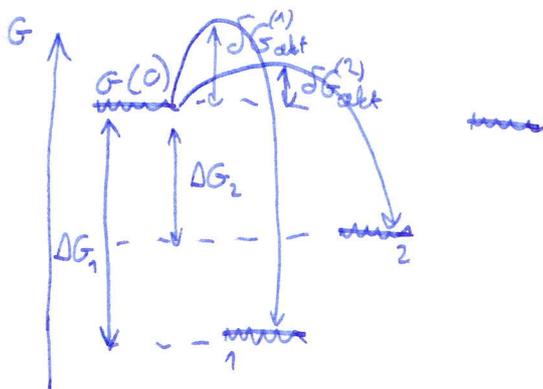
$G = \mu_1 n_1 + \mu_2 n_2$

$dG = \mu_1 dn_1 + \mu_2 dn_2 = [\mu_1 - \mu_2] dn_1 < 0$

$G_{min} = \mu_1 n_1^* + \mu_2 n_2^* \rightarrow n_1 \text{ max}, n_2 = 0 = \mu_1 n$



Merte meg a t.s.z?



leil.-ő energiájú állapotok

végző áll. \rightarrow Hamilton-elu

$\Delta G = \text{max}$
DE nem erre indul hanem

$\delta G = \text{min.} \rightarrow$ legkisebbségs felé

Clausius-Clapeyron: $\mu(T, P)$

$$p = f(T)$$

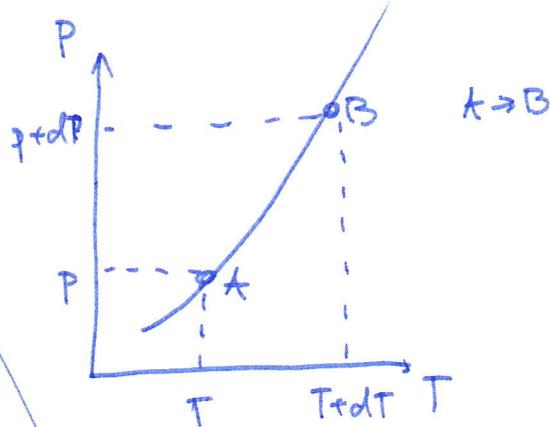
$$d\mu_1 = \left. \frac{\partial \mu_1}{\partial T} \right|_p dT + \left. \frac{\partial \mu_1}{\partial p} \right|_T dp =$$

$$= d\mu_2 = \left. \frac{\partial \mu_2}{\partial T} \right|_p dT + \left. \frac{\partial \mu_2}{\partial p} \right|_T dp$$

$$\frac{dp}{dT} = \frac{\left. \frac{\partial \mu_2}{\partial T} \right|_p - \left. \frac{\partial \mu_1}{\partial T} \right|_p}{\left. \frac{\partial \mu_2}{\partial p} \right|_T - \left. \frac{\partial \mu_1}{\partial p} \right|_T} = \frac{S_{M_2} - S_{M_1}}{V_{M_2} - V_{M_1}} \stackrel{\text{c.g.}}{\rightarrow} S_{M_2} - S_{M_1} = \frac{Q_{M_1,2}}{T} = \frac{L}{T}$$

$$G = \mu n \text{ (Euler eq)} \Rightarrow \mu = \frac{G(T, P)}{n} \frac{\partial \mu}{\partial T} = -\frac{S}{n} = -S_M$$

$$\frac{\partial \mu}{\partial p} = \frac{V}{n} = V_M$$



T5/4

$$dT(p, T, C)$$

$$dU, \delta Q = 0 \Rightarrow dS = 0$$

$$\text{I. f. f.: } dU = T dS - p dV \quad dU = -p dV$$

$$u(T, V) = \underbrace{\frac{\partial u}{\partial T}}_{C_V} dT + \frac{\partial u}{\partial V} dV$$

$$-p dU = C_V dT + \frac{\partial u}{\partial V} dV =$$

$$= C_V dT + T \frac{\partial p}{\partial T} dV - p dU \Rightarrow$$

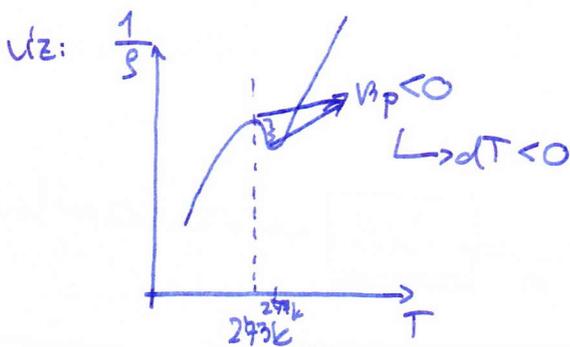
$$\Rightarrow C_V dT = -T \frac{V \beta_p}{\beta_T} dU$$

$$\boxed{dT = -T \frac{V \beta_p}{\beta_T C_V} dU}$$

$$\text{Trick: } dp(T, V) = \frac{\partial p}{\partial T} dT + \frac{\partial p}{\partial V} dV = 0 \text{ bei } dz=0$$

$$\text{elkine t\u00fcl\u00e9d\u00e9ni} \rightarrow \frac{\partial}{\partial T}$$

$$0 = \frac{\partial p}{\partial T} \frac{\partial T}{\partial T} + \frac{\partial p}{\partial V} \frac{\partial V}{\partial T} \Rightarrow \frac{\partial p}{\partial T} = \frac{V \beta_p}{\beta_T}$$

T5/6 $u(S, V) \checkmark p, T, H(S, U)$

$$dU = T dS - p dV \quad dU = \frac{\partial u}{\partial S} dS + \frac{\partial u}{\partial V} dV \Rightarrow$$

$$H = U + pV = U - \frac{\partial u}{\partial V} V$$

$$F = U - TS = U - \frac{\partial u}{\partial S} S$$

$$G = H - TS = U - TS + pV =$$

$$\phi = U - \mu N$$

T5/7 $u, T, V, dU \checkmark$ $C_p, \beta_p \checkmark$ $dS = ?$ $p = \text{all.}$

$$S(T, p) \Rightarrow dS = \underbrace{\frac{\partial S}{\partial T}}_? \Big|_p dT + \underbrace{\frac{\partial S}{\partial p}}_0 \Big|_T dp$$

wertierbar

$$\delta Q = m c_p dT = T dS$$

$$dS = \frac{m c_p}{T} dT = \frac{m c_p}{T} dU \frac{dT}{dV} = \frac{m c_p}{T} \frac{1}{V \beta_p}$$

es zavor keeg \rightarrow def. d'g'ia
b'it'it'el d'
vel

$$\hookrightarrow \frac{\partial S}{\partial T} = \frac{m c_p}{T}$$

$$dS(u, T, V, dU, C_p, \beta_p) = \frac{m c_p}{T V \beta_p} dU$$

T5/9 $f = a T \left(\frac{l}{l_0} - \left(\frac{l}{l_0} \right)^2 \right)$

a, $u(l) = u$

b, $dU, dF, dG = ?$

c, $T = \text{all.}$, $\Delta U = ?$, $\Delta Q_{l_0} = ?$ $l_0 \rightarrow 2l_0$

d, $T \uparrow$, ha $\delta Q = 0$

f: intensiv $p \rightarrow -f$
l: extensiv $v \rightarrow l$

$$a, \frac{\partial u}{\partial l} \Big|_T = f - T \frac{\partial f}{\partial T} \Big|_l = f - T \frac{f}{T} = \boxed{0}$$

valt: $\frac{\partial u}{\partial v} \Big|_T = T \frac{\partial p}{\partial T} \Big|_v - p$

$$\boxed{u(l) = u}$$

b, $dU = T dS + f dl$

$$dF = dU - d(TS) = -S dT + f dl$$

$$dG = dU - d(TS) - d(fl) = -S dT - l df$$

\downarrow
-p

c, $dU = \delta Q + \delta W_{\text{mech}}$

$T = \text{all.} \rightarrow u(l) = u$ $dU = 0 \rightsquigarrow \delta Q = -\delta W_{\text{mech}} = \boxed{-f dl} \Rightarrow \delta Q < 0 \Rightarrow \text{hül}$

$W = \int f dl \rightarrow \delta W = f dl$

$$\Delta Q = -\Delta W = - \int_{l_0}^{2l_0} f dl = - \int_{l_0}^{2l_0} a T \left(\frac{l}{l_0} - \left(\frac{l}{l_0} \right)^2 \right) dl = a T \left[-\frac{l^2}{2l_0} - \frac{l^3}{3l_0} \right]_{l_0}^{2l_0} = \boxed{-a T l_0 < 0}$$

d, $dU = \delta Q + \delta W = f dl$

$dU_{(T, l)} = \underbrace{\frac{\partial u}{\partial T}}_{c_p} dT + \underbrace{\frac{\partial u}{\partial l}}_0 dl$; $f dl = c_p dT \rightarrow \frac{\partial T}{\partial l} \Big|_S = \frac{f}{c_p}$

$c_p > 0$
 $f > 0$
 $dl > 0$

\Downarrow
 $dT > 0$

T5/10 $\epsilon_r(T), \Delta Q = ?$ $\left. \begin{array}{l} \sim E: \text{int} \\ \text{TD: } \underline{P}: \text{ext.} \rightarrow \text{makr. pol.} \\ (\text{ED: } \underline{P}: \text{pol. sűrűség}) \end{array} \right\} \begin{array}{l} -P \rightarrow \underline{E} \\ U \rightarrow \underline{P} \end{array}$

\underline{P}
 $\underline{E} \nearrow (D, \underline{E})$
 $T = \text{all.}$
 $dU = 0$

$$\Delta Q = dU - \delta W = dU - \underline{E} d\underline{P} \quad \underline{E} \parallel \underline{P} \rightarrow \underline{E} d\underline{P} = E dP$$

$$dU(T, P) = \left. \frac{\partial U}{\partial T} \right|_{P, V} dT + \left. \frac{\partial U}{\partial P} \right|_{T, V} dP + \left. \frac{\partial U}{\partial V} \right|_{T, P} dV$$

$$\left. \frac{\partial U}{\partial P} \right|_T = E - T \left. \frac{\partial E}{\partial T} \right|_P$$

$$\Delta Q = -T \left. \frac{\partial E}{\partial T} \right|_P dP + E dP - E dP$$

$\underline{D} = \epsilon \underline{E} \quad \epsilon = \epsilon_0 \epsilon_r \quad \underline{D} = \epsilon_0 \underline{E} + \underline{P}$ pol. sűrűség

$$\epsilon \underline{E} = \epsilon_0 \underline{E} + \underline{P} \rightarrow \underline{E} = \frac{P}{\epsilon_0(\epsilon_r - 1)} = \frac{P}{V \epsilon_0(\epsilon_r - 1)}$$

$$\left. \frac{\partial E}{\partial T} \right|_P = -\frac{P}{\epsilon_0 V} \frac{1}{(\epsilon_r(T) - 1)^2} \left. \frac{\partial \epsilon_r}{\partial T} \right|_P$$

tlh. $\epsilon_r(p) = \epsilon_r$

$$\Delta Q = \frac{T}{\epsilon_0(\epsilon_r - 1)^2 V} \left. \frac{\partial \epsilon_r}{\partial T} \right|_P dP$$

$$\Rightarrow \Delta Q = \frac{T}{\epsilon_0(\epsilon_r - 1)^2 V} \frac{\partial \epsilon_r}{\partial T} \frac{P^2}{2}$$

$$\Rightarrow \Delta Q = \frac{1}{2} T \frac{\partial \epsilon_r}{\partial T} \epsilon_0 E^2 V$$

\Leftrightarrow ezért melegendő a kondik

T6/1 $p = \text{all.}$

$L = \Delta Q_{\text{átalak}} = \Delta H$

I. f. t.: $dU = \delta Q - p dV$

$H = U + p dV \rightarrow dH = \delta Q + V dp$

$\delta Q - p dV = dU = dH - d(pV) = dH - \overset{p=\text{all.}}{dp} V - p dV = dH - p dV$

$\delta Q = dH$

$L = \Delta H$ / $\int \text{fázisátalak}$

latens hő

T6/2
 1 kg víz
 101.3 kPa = all.
 $U = 220V$
 $t = 36,2 \text{ perc}$
 $I = 5A$
 $T = \text{all.}$

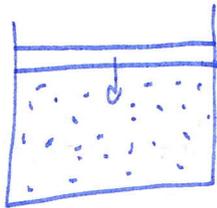
$\Delta H, \Delta S, \Delta U = ?$

$\Delta H = \Delta Q = \overset{\text{Joule-hő}}{U I t} = \boxed{2.257 \text{ MJ}}$
 $\Delta S = \int dS = \int \frac{\delta Q}{T} = \frac{1}{T} \int \delta Q = \frac{\Delta Q}{T} \approx \boxed{6 \frac{\text{kJ}}{\text{K}}}$

$\Delta U = \Delta Q - p \Delta V = \overset{\text{V gőz}}{\oplus} \rightarrow \overset{\text{V víz}}{U_{\text{viz}}}$
 $\Delta U = U_{\text{gőz}} - U_{\text{víz}} = U_{\text{gőz}}$
 $= \frac{M}{M} \frac{RT}{P}$

$\oplus = \Delta Q - p \frac{M}{M} \frac{RT}{P} = \Delta Q - \frac{M}{M} RT \approx \boxed{2 \text{ MJ}}$

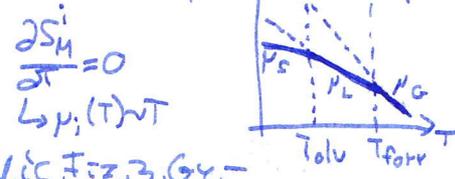
T6/3 $T_f = 100^\circ\text{C}$ gőz, id. g.
 $\Delta u = 0.7g$ víz
 $P_{\text{külső}} = \text{all.}$
 $\Delta W_{wi} = ?$



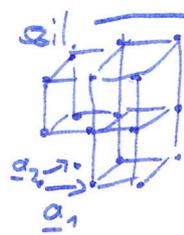
$\Delta W = -P_k \Delta V = -P_k (V_2 - V_1)$

$P_k V_1 = \frac{M}{M} RT_f$
 $P_k V_2 = \frac{M}{M} RT_f$
 $\Delta W = -P_k RT_f \frac{1}{M} (M_2 - M_1)$
 $= \boxed{120 \text{ kJ}}$

T6/4 $p_p(T)$
 $p = \text{all.}$
 1 komp $\mu(T)$
 $\frac{\partial S_M}{\partial T} = 0$
 $\hookrightarrow p_i(T) \sim T$
 $U_M = TS - pV + \mu M$
 $G = U - TS + pV = \mu M$
 $\frac{\partial G}{\partial T} \Big|_p = -S$



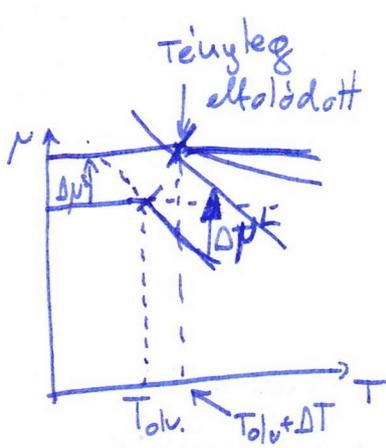
$\frac{\partial \mu}{\partial T} \Big|_p = -S_M$



$S_M^S < S_M^L < S_M^G$

3a, 6 kicsi
 léso
 össze.
 talvolso

TG/5



(11.30.)

Tolv. ↑ ha p ↑
 $V_M^S < V_M^L$

$$\left. \frac{\partial G}{\partial p} \right|_T = V \rightarrow \left. \frac{\partial \mu}{\partial p} \right|_T = V_M$$

Euler: Legendre: $G = \mu n$

$$\left. \frac{\partial \mu}{\partial p} \right|_T = V_M \sim \Delta \mu_i = V_M \Delta p$$

$$\left. \frac{\partial \mu}{\partial p} \right|_S < \left. \frac{\partial \mu}{\partial p} \right|_L$$

viz: $V_{M, H_2O}^S > V_{M, H_2O}^L$

$$T_{olv}(p + \Delta p) < T_{olv}(p)$$

TG/6

$$p = p_1 + \frac{L_M^{olv}}{\Delta V_M^{olv}} \ln \frac{T}{T_1}$$

T & p
 $T_1 \rightarrow p_1$

a, Biz.

b, lin. alizálás

Eggszerűség: $p_1 = p_2 = p$
 $T_1 = T_2 = T$

$$\mu_1(p, T) = \mu_2(p, T) = \mu(p, T)$$

$\hookrightarrow d\mu_1 = d\mu_2$ (eggszerűség: görbén)

$$\left. \frac{\partial \mu_1}{\partial p} \right|_T dp + \left. \frac{\partial \mu_1}{\partial T} \right|_p dT = \left. \frac{\partial \mu_2}{\partial p} \right|_T dp + \left. \frac{\partial \mu_2}{\partial T} \right|_p dT$$

V_{M2} S_{M2}

$$\mu = \frac{G}{n}$$

$$dG = dU + d(pV) - d(TS)$$

$$(S_{M2} - S_{M1}) dT = (V_{M2} - V_{M1}) dp$$

$$\frac{dp}{dT} = \frac{T}{T} \cdot \frac{S_{M2} - S_{M1}}{V_{M2} - V_{M1}} = \frac{L_M^{olv}}{T \Delta V_M^{olv}} \quad \underline{\underline{C-C}} \quad !$$

akkor tudjuk integrálni, ha
 $L_M^{olv}(T) = L_M^{olv}$ } közelítés
 $\Delta V_M^{olv}(T) = \Delta V_M^{olv}$ } korlátja

$$dp = \frac{L_M}{\Delta V_M} \frac{dT}{T} \quad //$$

$$dp' = \frac{L_M}{\Delta U_M} \frac{dT'}{T'} \quad \int_{p_1}^p dp' \quad \int_{T_1}^T dT'$$

$$p = p_1 + \frac{L_M}{\Delta U_M} \ln \frac{T}{T_1}$$

ha x=0

Linearizálás: kis hőm. vált. $T - T_1 \ll T_1 \Rightarrow \ln(1+x) \approx x$

ezt lehet linearizálni de nekünk ln... van

$$p = p_1 + \frac{L_M}{\Delta U_M} \ln \frac{T - T_1 + T_1}{T_1} \approx p_1 + \frac{L_M}{\Delta U_M} \frac{T - T_1}{T_1} \quad (\text{feltétel: } T \text{ közel } T_1 \text{-hez})$$

$$1 + \frac{T - T_1}{T_1} \quad \text{kéne: elég közel 0-hoz} \Rightarrow T - T_1 \ll T_1 \Rightarrow \frac{T - T_1}{T_1} \approx 0$$

TG/3

$p_0 = 1 \text{ bar}$

$T_{olv} = 83 \text{ K}$

$L_M^{olv} = 1176 \frac{\text{J}}{\text{mol}}$

$\Delta U_M^{olv} = 3,5 \frac{\text{cal}}{\text{mol}}$

$p_0 \uparrow, L_M = \text{all.}$

$\Delta U_M \sim T^{3/2} \rightarrow \Delta U_M = \Delta U_{M0} \left(\frac{T}{T_{olv}}\right)^{3/2}$

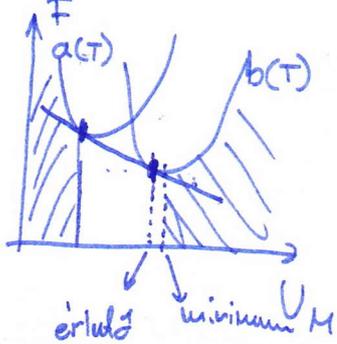
$p' = ?$, hőeg $T_{olv} \rightarrow 2T_{olv}$

$p_0 \uparrow p' = ?$

C-C: $\frac{dp}{dT} = \frac{L_M(T_{olv})^{3/2}}{T^{5/2} \Delta U_{M0}} \rightarrow dp = \frac{L_M(T_{olv})^{3/2}}{T^{5/2} \Delta U_{M0}} dT$

$p' = p_0 + \frac{L_M T_{olv}^{3/2}}{\Delta U_{M0}} \left[+ \frac{2}{3} T^{-3/2} \right]_{T_{olv}}^{2T_{olv}} = p_0 + \frac{L_M T_{olv}^{3/2}}{3 \Delta U_{M0} T_{olv}^{3/2}} \left[1 - \left(\frac{1}{2}\right)^{3/2} \right] \approx 1,56 \text{ bar}$

TG/10
T.T.:
TG/7,8



$p, T, \mu \Rightarrow$ azonos

interjúk azonosak a fázisokban \rightarrow egy a, b fázisok

$T \checkmark$
 $\mu \checkmark$
 $p-T$ kell meghatározni

$$\left. \frac{\partial F}{\partial V} \right|_T = \left. \frac{\partial F_M}{\partial V_M} \right|_T = -p \quad (\Leftarrow \text{F.E. alapján})$$

\rightarrow azonos meredekség, ha egyensúly
másképp: érintők // -ak

$$G = \mu n = F + pV$$

$$\mu_a = \mu_b = F_M^i + pV_M^i$$

$$\rightarrow -p = \frac{F_M^b - F_M^a}{V_M^b - V_M^a}$$

\rightarrow egyensúly
 \downarrow
összekötő egyenesen van

$V_M < V_M^a \Rightarrow$ csak a fázis

$V_M > V_M^b \Rightarrow$ csak b fázis

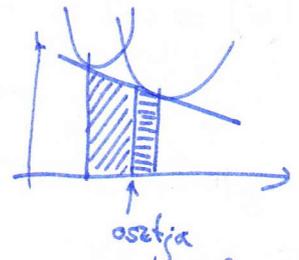
$V_M^a < V_M < V_M^b \Rightarrow$ a és b is jelen van

rel. koncentráció: $x \in [0, 1]: a; b: 1-x$

$$F_M = xF_{Ma}^* + (1-x)F_{Mb}^*$$

$$\frac{V_M - V_{Mb}}{V_{Ma} - V_M} = \frac{x}{1-x}$$

Mérleg szabály



az egyik komponensre is,
nem csak fázisokra

FIZIKAI TALALKULÁSOK

elsőrendű

μ elsőrendű deriváltjai ugranak

$$\left. \begin{aligned} -\frac{\partial \mu}{\partial T} \Big|_p &= S_M \\ -\frac{\partial \mu}{\partial p} \Big|_T &= V_M \end{aligned} \right\} \begin{aligned} S_M^A + S_M^B \\ V_M^A + V_M^B \end{aligned}$$

másodrendű (folytonos)

μ másodrendű deriváltjai ugranak

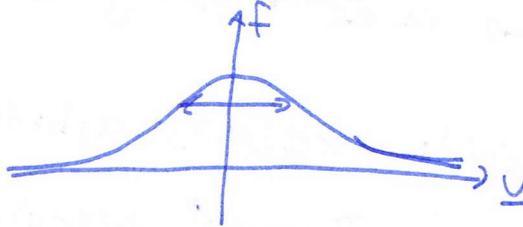
$$\begin{aligned} \frac{\partial^2 \mu}{\partial p^2} \Big|_T &= \frac{\partial V}{\partial p} \Big|_T = -V\kappa_T \\ \frac{\partial^2 \mu}{\partial T^2} \Big|_p &= -\frac{C_p}{T} \\ \frac{\partial^2}{\partial T \partial p} &= U\beta_p \end{aligned}$$

↓
 mérhető mennyiségek ugranak
 (de μ folytonos \Rightarrow törés)

TG/11

Mx-seloszlás:

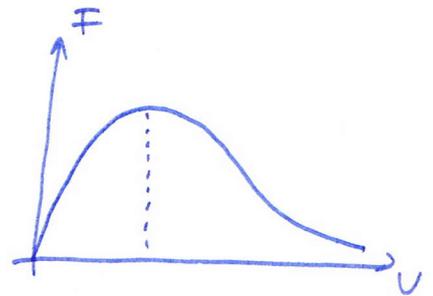
$$f(v) = \sqrt{\frac{m}{2\pi k_B T}}^3 e^{-\frac{mv^2}{2k_B T}}$$



seb. nagys.-ra vonatkozó eloszlás

$$F(v) = 4\pi v^2 f(v) = 4\pi v^2 \sqrt{\frac{m}{2\pi k_B T}}^3 e^{-\frac{mv^2}{2k_B T}}$$

\swarrow térfogat \searrow valószínűség
 gömbhéjra indultunk $v, v+dv$ közt



$F(v) = \text{max}$

$\ln F(v) = \text{max}$, mert 1-1 értéke függ. de $\ln F(v) = \text{max} \quad / \frac{\partial}{\partial v^2}$

$$\hookrightarrow v_c = \sqrt{\frac{2k_B T}{m}}$$

$\bar{v} = \int_0^{\infty} F(v) v dv = \sqrt{\frac{8k_B T}{m}}$

↓
várható érték

$\bar{v}^2 = 3 \bar{v}_x^2 = 3 \frac{k_B T}{m}$

↓
izotróp a tér, 1 irányra számolunk

T1/3

$w = \frac{1}{2} m v^2 \rightarrow v = \sqrt{\frac{2w}{m}}$ (dv miatt számoljuk)

$f(w) \Rightarrow$ energia classis = ?
sűrűség

$F(v) dv = f(w) dw$

normatertő
lekepezés
miatt szorozzuk
dv-vel

$\frac{dv}{dw} = \sqrt{\frac{2}{m}} \frac{1}{2} \sqrt{\frac{1}{w}} \rightarrow dv = \frac{dw}{\sqrt{2mw}}$

$A \cdot \left(\frac{v}{v_0}\right)^2 e^{-\left(\frac{v}{v_0}\right)^2}$

↓ dim.-tanítjuk
A és v_0 új const.-ok

→ még ~~ebből~~ constok: $B = \frac{A}{v_0 \sqrt{2m}}$
 $v_0 = \frac{1}{2} m v_0^2$

$f(w) = B \cdot \sqrt{w}$ \uparrow v^2 -esből \uparrow $-w/w_0$ $\frac{dw}{\sqrt{2mw}} \Rightarrow f(w) = B \sqrt{w} e^{-w/w_0} \rightarrow w_0 \text{ max?}$

$f(w) dw = A \left(\frac{w}{w_0}\right) e^{-\frac{w}{w_0}}$ Gaussból

$\left. \frac{df(w)}{dw} \right|_{w_0} = 0 = B e^{-w_0/k_B T} \left(\frac{1}{2\sqrt{w_0}} - \frac{\sqrt{w_0}}{k_B T} \right)$

$0 \Rightarrow w_0 = \frac{k_B T}{2}$

$\bar{w} = \int_0^{\infty} w f(w) dw = B \int_0^{\infty} w^{3/2} e^{-w/k_B T} dw \Rightarrow$ parc.-an kiszámolni?

T1/2

entropia \rightarrow fázisátal + max. relaxálás

$\bar{c}_v = \frac{3}{2} k_B$

